

Dual Micropower DC/DC Converters with Schottky Diodes

FEATURES

- Generates Well-Regulated Positive and Negative Outputs
- Low Quiescent Current: 20µA (per Converter) in Active Mode <1µA in Shutdown Mode
- Internal 42V Power Switches
- Internal 42V Schottky Diodes
- Low V_{CESAT} Switch: 180mV at 150mA
- Input Voltage Range: 2.4V to 15V
 High Output Voltages: Up to ±40V
- Low Profile (0.8mm) 3mm x 3mm DFN Package

APPLICATIONS

- CCD Bias
- LCD Bias
- Handheld Computers
- Digital Cameras

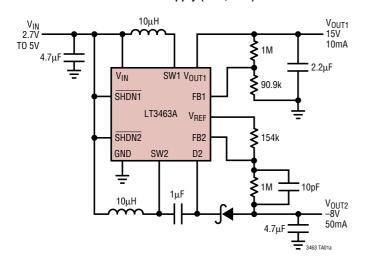
DESCRIPTION

The LT[®]3463/LT3463A are dual micropower DC/DC converters with internal Schottky diodes in a 10-lead $3 \text{mm} \times$ 3mm DFN package. Negative and positive LT3463 converters have a 250mA current limit. The LT3463A positive converter also has a 250mA limit, while the negative converter has a 400mA limit. Both devices have an input voltage range of 2.4V to 15V, making them ideal for a wide variety of applications. Each converter features a guiescent current of only 20µA, which drops to under 1µA in shutdown. A current limited, fixed off-time control scheme conserves operating current, resulting in high efficiency over a broad range of load current. The 42V switch enables high voltage outputs up to $\pm 40V$ to be easily generated without the use of costly transformers. The low 300ns offtime permits the use of tiny, low profile inductors and capacitors to minimize footprint and cost in space-conscious portable applications.

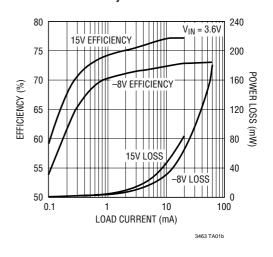
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TYPICAL APPLICATION

CCD Bias Supply (15V, -8V)



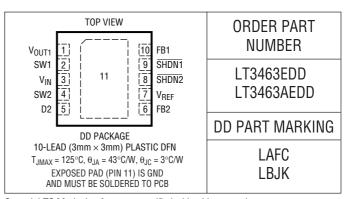
Efficiency and Power Loss



ABSOLUTE MAXIMUM RATINGS

(Note 1)		
V _{IN} , SHDN1	, SHDN2 Voltage	15V
SW1, SW2,	V _{OUT1} Voltage	42V
D2 Voltage .		42V
FB1, FB2 Vo	oltage Range	0.3V to 2V
Junction Te	mperature	125°C
Operating A	mbient Temperature Range	
(Note 2).		40°C to 85°C
	nperature Range	

PACKAGE/ORDER INFORMATION



Consult LTC Marketing for parts specified with wider operating temperature ranges.

ELECTRICAL CHARACTERISTICS The \bullet denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^{\circ}C$. $V_{IN} = 2.5V$, $V_{\overline{SHDN}} = 2.5V$ unless otherwise noted.

Minimum Input Voltage	PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
Shutdown Current V _{SHDN1} = V _{SHDN2} = 0V 0.1 1 μA V _{REF} Pin Voltage With $124k\Omega$ to GND • 1.23 1.25 1.27 V V _{REF} Pin Voltage High to Low Transition • 1.225 1.25 1.27 V FB1 Comparator Trip Voltage High to Low Transition • 1.225 1.25 1.275 V FB1 Comparator Hysteresis 8 mV 0.05 0.10 %/V FB1 Pin Bias Current (Note 3) V _{FB1} = 1.3V • 0.05 0.10 %/V FB2 Comparator Trip Voltage Low to High Transition • 0 3 12 mV FB2 Comparator Hysteresis 8 mV W 0.05 0.10 %/V FB2 Pin Bias Current (Note 4) V _{FB1} = -0.1V 0.05 0.10 %/V FB2 Pin Bias Current (Note 4) V _{FB2} = -0.1V 0.05 0.10 %/V FB2 Pin Bias Current (Note 4) V _{FB2} = -0.1V 0.05 0.10 mA SW1 Switch Off Time V _{OUTT} - V _N = 4V 0.00 1.5 μS	Minimum Input Voltage				2.2	2.4	V
VREF Pin Voltage With 124kΩ to GND 1.23 1.25 1.27 V VREF Pin Voltage Line Regulation With 124kΩ to GND 0.05 0.10 %/V FB1 Comparator Trip Voltage High to Low Transition • 1.225 1.25 1.275 V FB1 Comparator Hysteresis 8 mV FB1 Line Regulation 2.5V < V _{IN} < 15V	Total Quiescent Current	For Both Switchers, Not Switching			40	60	μΑ
VREF Pin Voltage Line Regulation With 124kΩ to GND 0.05 0.10 %/V FB1 Comparator Trip Voltage High to Low Transition ■ 1.225 1.25 1.25 V FB1 Comparator Hysteresis 8 mV FB1 Line Regulation 2.5V < V _{IN} < 15V	Shutdown Current	$V_{\overline{SHDN1}} = V_{\overline{SHDN2}} = 0V$			0.1	1	μΑ
FB1 Comparator Trip Voltage	V _{REF} Pin Voltage	With 124kΩ to GND	•	1.23	1.25	1.27	V
FB1 Comparator Hysteresis 8 mV	V _{REF} Pin Voltage Line Regulation	With 124kΩ to GND			0.05	0.10	%/V
FB1 Line Regulation 2.5V < V _{IN} < 15V 0.05 0.10 %/V FB1 Pin Bias Current (Note 3) V _{FB1} = 1.3V ● 20 50 nA FB2 Comparator Trip Voltage Low to High Transition ● 0 3 12 mV FB2 Comparator Hysteresis 8 mV mV 0.05 0.10 %/V FB2 Line Regulation (V _{REF} - V _{FB2}) 2.5V < V _{IN} < 15V	FB1 Comparator Trip Voltage	High to Low Transition	•	1.225	1.25	1.275	V
FB1 Pin Bias Current (Note 3) $V_{FB1} = 1.3V$ 0 20 50 nA FB2 Comparator Trip Voltage Low to High Transition 0 3 12 mV FB2 Comparator Hysteresis 8 mV FB2 Line Regulation ($V_{REF} - V_{FB2}$) 2.5V < $V_{IN} < 15V$ 0.05 0.10 %/V FB2 Pin Bias Current (Note 4) $V_{FB2} = -0.1V$ 0 20 50 nA SW1 Switch Off Time $V_{0UT1} - V_{IN} = 4V$ 300 ns SW2 Switch Off Time $V_{FB2} = 0.1V$ 300 ns Switch VCESAT (SW1, SW2) $I_{SW} = 150mA$ 180 mV Switch Current Limit (SW1) 180 250 320 mA Switch Current Limit (SW2) LT3463 180 250 320 mA Swith Leakage Current (SW1, SW2) Switch Off, $V_{SW} = 42V$ 0.01 1 μ A Schottky Reverse Leakage Current $V_{OUT1} - V_{SW} = 42V$ 1 5 μ A ShDN1 Pin Current $V_{SHDN1} = 2.5V$ 4 10 μ A <td>FB1 Comparator Hysteresis</td> <td></td> <td></td> <td></td> <td>8</td> <td></td> <td>mV</td>	FB1 Comparator Hysteresis				8		mV
FB2 Comparator Trip Voltage Low to High Transition ● 0 3 12 mV FB2 Comparator Hysteresis 8 mV FB2 Line Regulation (V _{REF} − V _{FB2}) 2.5V < V _{IN} < 15V	FB1 Line Regulation	2.5V < V _{IN} < 15V			0.05	0.10	%/V
FB2 Comparator Hysteresis 8 mV FB2 Line Regulation (V _{REF} − V _{FB2}) 2.5V < V _{IN} < 15V	FB1 Pin Bias Current (Note 3)	V _{FB1} = 1.3V	•		20	50	nA
FB2 Line Regulation (V _{REF} − V _{FB2}) 2.5V < V _{IN} < 15V 0.05 0.10 %/V FB2 Pin Bias Current (Note 4) V _{FB2} = −0.1V • 20 50 nA SW1 Switch Off Time V _{OUT1} − V _{IN} = 4V V _{OUT1} − V _{IN} = 0V 300 ns SW2 Switch Off Time V _{FB2} < 0.1V V _{VFB2} = 1V 300 ns Switch V _{CESAT} (SW1, SW2) I _{SW} = 150mA 180 mV Switch Current Limit (SW1) 180 250 320 mA Switch Current Limit (SW2) LT3463 LT3463A 180 250 320 mA Swith Leakage Current (SW1, SW2) Switch Off, V _{SW} = 42V 0.01 1 μA Schottky Forward Voltage (V _{OUT1} , D2) I _D = 150mA 750 mV Schottky Reverse Leakage Current V _{OUT1} − V _{SW} = 42V V _{D2} = −42V 1 5 μA SHDN1 Pin Current V _{SHDN1} = 2.5V 4 10 μA SHDN2 Pin Current V _{SHDN2} = 2.5V 4 10 μA	FB2 Comparator Trip Voltage	Low to High Transition	•	0	3	12	mV
FB2 Pin Bias Current (Note 4) $V_{FB2} = -0.1V$ 0 20 50 nA SW1 Switch Off Time $V_{OUT1} - V_{IN} = 4V$ 300 ns SW2 Switch Off Time $V_{FB2} < 0.1V$ 300 ns Switch V _{CESAT} (SW1, SW2) $I_{SW} = 150$ mA 180 mV Switch Current Limit (SW1) 180 250 320 mA Switch Current Limit (SW2) LT3463 180 250 320 mA Swith Leakage Current (SW1, SW2) Switch Off, V _{SW} = 42V 0.01 1 μA Schottky Forward Voltage (V _{OUT1} , D2) $I_D = 150$ mA 750 mV Schottky Reverse Leakage Current $V_{OUT1} - V_{SW} = 42V$ 1 5 μA SHDN1 Pin Current $V_{SHDN1} = 2.5V$ 4 10 μA SHDN2 Pin Current $V_{SHDN2} = 2.5V$ 4 10 μA	FB2 Comparator Hysteresis				8		mV
SW1 Switch Off Time $V_{OUT1} - V_{IN} = 4V$ $V_{OUT1} - V_{IN} = 0V$ 300 $I_{I.5}$ ns $I_{I.5}$ SW2 Switch Off Time $V_{FB2} < 0.1V$ $V_{FB2} = 1V$ 300 $I_{I.5}$ ns $I_{I.5}$ Switch V_{CESAT} (SW1, SW2) $I_{SW} = 150 \text{mA}$ 180 $I_{I.5}$ mV Switch Current Limit (SW1) 180 $I_{I.5}$ 250 $I_{I.5}$ mA Switch Current Limit (SW2) LT3463 $I_{I.5}$ 180 $I_{I.5}$ 250 $I_{I.5}$ mA Switch Leakage Current (SW1, SW2) Switch Off, $V_{SW} = 42V$ 0.01 $I_{I.5}$ mA Schottky Forward Voltage (V_{OUT1} , D2) $I_{I.5}$ = 150mA 750 $I_{I.5}$ mV Schottky Reverse Leakage Current $V_{OUT1} - V_{SW} = 42V$ $V_{D2} = -42V$ 1 $I_{I.5}$ $I_{I.5}$ $I_{I.5}$ SHDN1 Pin Current $I_{I.5}$ = 150mA 4 $I_{I.5}$ $I_{I.5}$ $I_{I.5}$ $I_{I.5}$ SHDN2 Pin Current $I_{I.5}$ = 150mA 4 $I_{I.5}$	FB2 Line Regulation (V _{REF} – V _{FB2})	2.5V < V _{IN} < 15V			0.05	0.10	%/V
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	FB2 Pin Bias Current (Note 4)	$V_{FB2} = -0.1V$	•		20	50	nA
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	SW1 Switch Off Time						ns
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							μs
Switch V _{CESAT} (SW1, SW2) I_{SW} = 150mA 180 mV Switch Current Limit (SW1) 180 250 320 mA Switch Current Limit (SW2) LT3463 LT3463A 180 250 320 mA Swith Leakage Current (SW1, SW2) Switch Off, V _{SW} = 42V 0.01 1 μ A Schottky Forward Voltage (V _{OUT1} , D2) I_D = 150mA 750 mV Schottky Reverse Leakage Current $V_{OUT1} - V_{SW} = 42V$ 1 5 μ A SHDN1 Pin Current V_{SHDN1} = 2.5V 4 10 μ A SHDN2 Pin Current V_{SHDN2} = 2.5V 4 10 μ A	SW2 Switch Off Time	V _{FB2} < 0.1V					
Switch Current Limit (SW1) 180 250 320 mA Switch Current Limit (SW2) LT3463 180 250 320 mA Swith Leakage Current (SW1, SW2) Switch Off, V _{SW} = 42V 0.01 1 μA Schottky Forward Voltage (V _{OUT1} , D2) I _D = 150mA 750 mV Schottky Reverse Leakage Current V _{OUT1} - V _{SW} = 42V 1 5 μA V _{D2} = -42V 1 5 μA SHDN1 Pin Current V _{SHDN1} = 2.5V 4 10 μA SHDN2 Pin Current V _{SHDN2} = 2.5V 4 10 μA	Contab V (CM/4 CM/0)						
Switch Current Limit (SW2)LT3463 LT3463A180 320250 400320 460mASwith Leakage Current (SW1, SW2)Switch Off, $V_{SW} = 42V$ 0.011 μ ASchottky Forward Voltage (V_{OUT1} , D2) $I_D = 150mA$ 750mVSchottky Reverse Leakage Current $V_{OUT1} - V_{SW} = 42V$ $V_{D2} = -42V$ 15 μ ASHDN1 Pin Current $V_{SHDN1} = 2.5V$ 410 μ ASHDN2 Pin Current $V_{SHDN2} = 2.5V$ 410 μ A		ISW = 150MA		400		000	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$							
Swith Leakage Current (SW1, SW2)Switch Off, $V_{SW} = 42V$ 0.011 μA Schottky Forward Voltage (V_{OUT1} , D2) $I_D = 150 \text{mA}$ 750mVSchottky Reverse Leakage Current $V_{OUT1} - V_{SW} = 42V$ $V_{D2} = -42V$ 15 μA SHDN1 Pin Current $V_{SHDN1} = 2.5V$ 410 μA SHDN2 Pin Current $V_{SHDN2} = 2.5V$ 410 μA	Switch Current Limit (SW2)	1 - 1 - 1 - 1					
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Schottky Reverse Leakage Current $V_{OUT1} - V_{SW} = 42V$ $V_{D2} = -42V$ 15 μA SHDN1 Pin Current $V_{\overline{SHDN1}} = 2.5V$ 410 μA SHDN2 Pin Current $V_{\overline{SHDN2}} = 2.5V$ 410 μA						l	
VD2 = -42V 1 5 μA SHDN1 Pin Current VSHDN1 = 2.5V 4 10 μA SHDN2 Pin Current VSHDN2 = 2.5V 4 10 μA		I _D = 150mA			750		mV
SHDN1 Pin Current $V_{\overline{SHDN1}} = 2.5V$ 410 μA SHDN2 Pin Current $V_{\overline{SHDN2}} = 2.5V$ 410 μA	Schottky Reverse Leakage Current				1 1		
$\frac{\text{SHDN2 Pin Current}}{\text{V}_{\overline{S}\overline{H}\overline{D}\overline{N}2}} = 2.5 \text{V} \qquad \qquad 4 \qquad 10 \qquad \mu \text{A}$	SHDN1 Pin Current				4		
OHDIAL TO PARTIE THE P							
SHDN1/SHDN2 Start-Up Threshold 0.3 1 1.5 V	SHDN1/SHDN2 Start-Up Threshold	- OHDINZ		0.3			V

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

Note 2: The LT3463/LT3463A are guaranteed to meet performance specifications from 0° C to 70° C. Specifications over the -40° C to 85° C

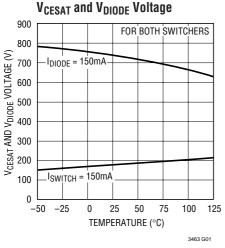
operating ambient temperature range are assured by design, characterization and correlation with statistical process controls.

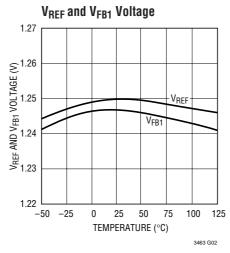
Note 3: Bias current flows into the FB1 pin.

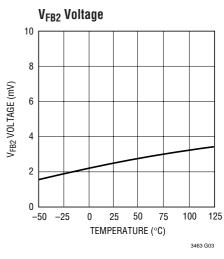
Note 4: Bias current flows out of the FB2 pin.

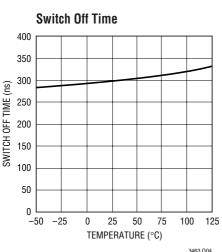
/ LINEAR

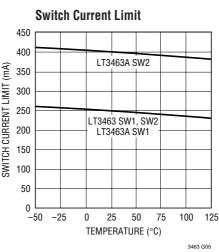
TYPICAL PERFORMANCE CHARACTERISTICS

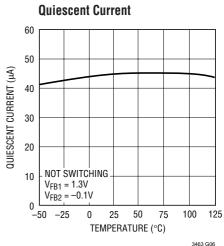












PIN FUNCTIONS

V_{OUT1} (**Pin 1**): Output Voltage Switcher 1. This is the cathode of an internal Schottky diode whose anode is connected to the SW1 pin.

SW1 (**Pin 2**): Switch Pin for Switcher 1. This is the collector of the internal NPN switch. Minimize the metal trace area connected to this pin to minimize EMI.

V_{IN} (**Pin 3**): Input Supply Pin. Bypass this pin with a capacitor as close to the device as possible.

SW2 (**Pin 4**): Switch Pin for Switcher 2. This is the collector of the internal NPN switch. Minimize the metal trace area connected to this pin to minimize EMI.

D2 (**Pin 5**): Diode for Switcher 2. This is the anode of an internal Schottky diode whose cathode connected to the GND pin.

FB2 (Pin 6): Feedback Pin for Switcher 2. Set the output voltage by selecting values for R3 and R4.

V_{REF} (**Pin 7**): Voltage Reference Pin (1.25V). This pin is used along with FB2 to set the negative output voltage for Switcher 2.

SHDN2 (Pin 8): Shutdown Pin for Switcher 2. Pull this pin above 1.5V to enable Switcher 2. Pull below 0.3V to turn it off. Do not leave this pin floating.





PIN FUNCTIONS

SHDN1 (**Pin 9**): Shutdown Pin for Switcher 1. Pull this pin above 1.5V to enable Switcher 1. Pull below 0.3V to turn it off. Do not leave this pin floating.

FB1 (Pin 10): Feedback Pin for Switcher 1. Set the output voltage by selecting values for R1 and R2.

GND (Pin 11): Exposed Pad. Solder this exposed pad directly to the local ground plane. This pad must be electrically connected for proper operation.

BLOCK DIAGRAM

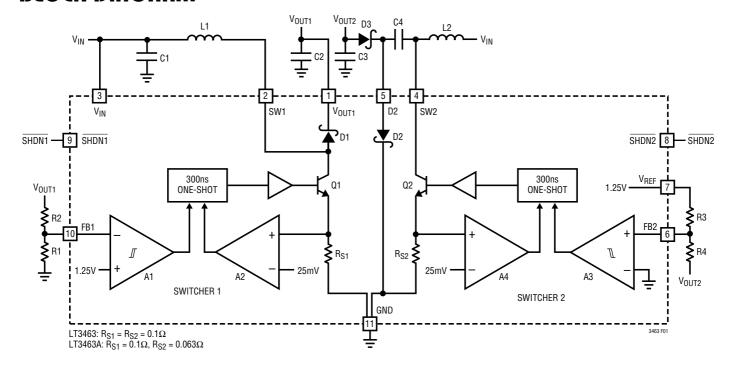


Figure 1. Block Diagram

OPERATION

The LT3463 uses a constant off-time control scheme to provide high efficiency over a wide range of output current. Operation can be best understood by referring to the block diagram in Figure 1. When the voltage at the FB1 pin is slightly above 1.25V, comparator A1 disables most of the internal circuitry. Output current is then provided by capacitor C2, which slowly discharges until the voltage at the FB1 pin goes below the hysteresis point of A1 (typical hysteresis at the FB1 pin is 8mV). A1 then enables the internal circuitry, turns on power switch Q1, and the

current in inductor L1 begins ramping up. Once the switch current reaches 250mA, comparator A2 resets the one-shot, which turns off Q1 for 300ns. Q1 turns on again and the inductor currents ramp back up to 250mA, then A2 again resets the one-shot. This switching action continues until the output voltage is charged up (until the FB1 pin reaches 1.25V), then A1 turns off the internal circuitry and the cycle repeats. The second switching regulator is an inverting converter (which generates a negative output) but the basic operation is the same.

LINEAR

APPLICATIONS INFORMATION

Choosing an Inductor

Several recommended inductors that work well with the LT3463 are listed in Table 1, although there are many other manufacturers and devices that can be used. Consult each manufacturer for more detailed information and for their entire selection of related parts. Many different sizes and shapes are available. Use the equations and recommendations in the next few sections to find the correct inductance value for your design.

Table 1. Recommended Inductors

PART	L (µH)	MAX I _{DC} (mA)	$\frac{\text{MAX}}{\text{DCR}(\Omega)}$	HEIGHT (mm)	MANUFACTURER
CMD4D06	4.7 10 22	750 500 310	0.22 0.46 1.07	0.8	Sumida (847) 956-0666 www.sumida.com
CDRH3D16	10 22	500 310	0.19 0.36	1.8	Sumida
LP04812	4.7 10 22	600 400 280	0.16 0.30 0.64	1.2	Coilcraft (847) 639-6400 www.coilcraft.com
LQH32C	10 15 22	450 300 250	0.39 0.75 0.92	1.8	Murata (714) 852-2001 www.murata.com
LQH31C	4.7	340	0.85	1.8	Murata

Inductor Selection—Boost Regulator

The formula below calculates the appropriate inductor value to be used for a boost regulator using the LT3463 (or at least provides a good starting point). This value provides a good tradeoff in inductor size and system performance. Pick a standard inductor close to this value. A larger value can be used to slightly increase the available output current, but limit it to around twice the value calculated below, as too large of an inductance will increase the output voltage ripple without providing much additional output current. A smaller value can be used (especially for systems with output voltages greater than 12V) to give a smaller physical size. Inductance can be calculated as:

$$L = \frac{V_{OUT} - V_{IN(MIN)} + V_{D}}{I_{LIM}} t_{OFF}$$

where V_D = 0.5V (Schottky diode voltage), I_{LIM} = 250mA (or 400mA) and t_{OFF} = 300ns; for designs with varying V_{IN}

such as battery powered applications, use the minimum V_{IN} value in the above equation. For most regulators with output voltages below 7V, a 4.7 μ H inductor is the best choice, even though the equation above might specify a smaller value.

For higher output voltages, the formula above will give large inductance values. For a 3V to 20V converter (typical LCD Bias application), a $21\mu H$ inductor is called for with the above equation, but a $10\mu H$ inductor could be used without much reduction in the maximum output current.

Inductor Selection—Inverting Regulator

The formula below calculates the appropriate inductor value to be used for an inverting regulator using the LT3463 (or at least provides a good starting point). This value provides a good tradeoff in inductor size and system performance. Pick a standard inductor close to this value (both inductors should be the same value). A larger value can be used to slightly increase the available output current, but limit it to around twice the value calculated below, as too large of an inductance will increase the output voltage ripple without providing much additional output current. A smaller value can be used (especially for systems with output voltages greater than 12V) to give a smaller physical size. Inductance can be calculated as:

$$L = 2 \left(\frac{\left| V_{OUT} \right| + V_{D}}{I_{LIM}} \right) t_{OFF}$$

where $V_D = 0.5V$ (Schottky diode voltage), $I_{LIM} = 250mA$ (or 400mA) and $t_{OFF} = 300ns$.

For higher output voltages, the formula above will give large inductance values. For a 3V to 20V converter (typical LCD bias application), a $49\mu H$ inductor is called for with the above equation, but a $10\mu H$ or $22\mu H$ inductor could be used without much reduction in the maximum output current.

Inductor Selection—Inverting Charge Pump Regulator

For the inverting regulator, the voltage seen by the internal power switch is equal to the sum of the absolute value of the input and output voltages, so that generating high



3463

APPLICATIONS INFORMATION

output voltages from a high input voltage source will often exceed the 50V maximum switch rating. For instance, a 12V to –40V converter using the inverting topology would generate 52V on the SW pin, exceeding its maximum rating. For this application, an inverting charge pump is the best topology.

The formula below calculates the approximate inductor value to be used for an inverting charge pump regulator using the LT3463. As for the boost inductor selection, a larger or smaller value can be used. For designs with varying V_{IN} such as battery powered applications, use the minimum V_{IN} value in the equation below.

$$L = \frac{\left|V_{OUT}\right| - V_{IN(MIN)} + V_{D}}{I_{IIM}} t_{OFF}$$

Capacitor Selection

The small size and low ESR of ceramic capacitors makes them ideal for LT3463 applications. Use only X5R and X7R types because they retain their capacitance over wider voltage and temperature ranges than other ceramic types. A 1 μ F input capacitor and a 0.22 μ F or 0.47 μ F output capacitor are sufficient for most applications. Table 2 shows a list of several ceramic capacitor manufacturers. Consult the manufacturers for more detailed information on their entire selection of ceramic capacitors. For applications needing very low output voltage ripple, larger output capacitor values can be used.

Table 2. Recommended Ceramic Capacitor Manufacturers

• • • • • • • • • • • • • • • • • • •			
MANUFACTURER	PHONE	URL	
AVX	843-448-9411	www.avxcorp.com	
Kemet	408-986-0424	www.kemet.com	
Murata	814-237-1431	www.murata.com	
Taiyo Yuden	408-573-4150	www.t-yuden.com	

Inrush Current

When V_{IN} is increased from ground to operating voltage while the output capacitor is discharged, an inrush current will flow through the inductor and integrated Schottky diode into the output capacitor. Conditions that increase

inrush current include a larger more abrupt voltage step at V_{IN} , a larger output capacitor tied to the outputs, and an inductor with a low saturation current.

While the internal diode is designed to handle such events, the inrush current should not be allowed to exceed 1 amp. For circuits that use output capacitor values within the recommended range and have input voltages of less than 5V, inrush current remains low, posing no hazard to the device. In cases where there are large steps at V_{IN} and/or a large capacitor is used at the outputs, inrush current should be measured to ensure safe operation.

Setting the Output Voltages

The output voltages are programmed using two feedback resistors. As shown in Figure 1, resistors R1 and R2 program the positive output voltage (for Switcher 1), and resistors R3 and R4 program the negative output voltage (for Switcher 2) according to the following formulas:

$$V_{OUT1} = 1.25V \left(1 + \frac{R2}{R1} \right)$$

$$V_{OUT2} = -1.25V \left(\frac{R4}{R3} \right)$$

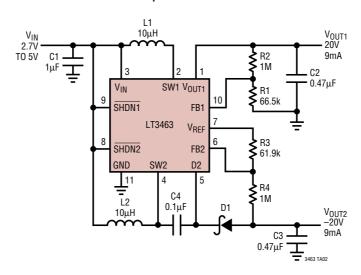
R1 and R3 are typically 1% resistors with values in the range of 50k to 250k.

Board Layout Considerations

As with all switching regulators, careful attention must be paid to the PCB board layout and component placement. To maximize efficiency, switch rise and fall times are made as short as possible. To prevent electromagnetic interference (EMI) problems, proper layout of the high frequency switching path is essential. The voltage signal of the SW pin has sharp rising and falling edges. Minimize the length and area of all traces connected to the SW pin and always use a ground plane under the switching regulator to minimize interplane coupling. In addition, the ground connection for the feedback resistor R1 should be tied directly to the GND pin and not shared with any other component, ensuring a clean, noise-free connection.

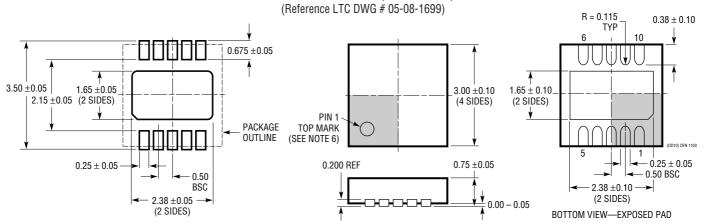
TYPICAL APPLICATION

Dual Output ±20V Converter



PACKAGE DESCRIPTION

DD Package 10-Lead Plastic DFN (3mm × 3mm)



RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS

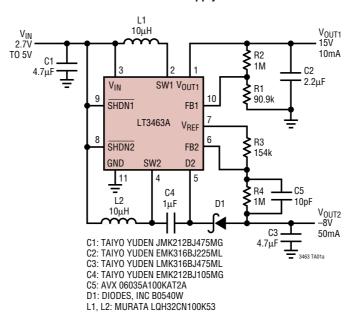
NOTE:

- 1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE MO-229 VARIATION OF (WEED-2). CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT
- 2. DRAWING NOT TO SCALE
- 3. ALL DIMENSIONS ARE IN MILLIMETERS
- 4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
- 5. EXPOSED PAD SHALL BE SOLDER PLATED 6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE



TYPICAL APPLICATION

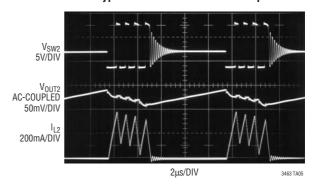
CCD Bias Supply



Typical Waveforms for 15V Output

V_{SW1} 10V/DIV V_{OUT1} AC-COUPLED 50mV/DIV 1L1 200mA/DIV 2µs/DIV 3463 TA04

Typical Waveforms for -8V Output



RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LT1615/LT1615-1	300mA/80mA (I _{SW}), High Efficiency Step-Up DC/DC Converters	V _{IN} : 1V to 15V, V _{OUT(MAX)} : 34V, I _Q : 20μA, I _{SD} : <1μA, ThinSOT Package
LT1944	Dual Output 350mA (I _{SW}), Constant Off-Time, High Efficiency Step-Up DC/DC Converter	$V_{IN}\!\!:$ 1.2V to 15V, $V_{OUT(MAX)}\!\!:$ 34V, $I_{Q}\!\!:$ 20 μ A, $I_{SD}\!\!:$ <1 μ A, MS Package
LT1944-1	Dual Output 150mA (I _{SW}), Constant Off-Time, High Efficiency Step-Up DC/DC Converter	$V_{IN}\!\!:$ 1.2V to 15V, $V_{OUT(MAX)}\!\!:$ 34V, $I_{Q}\!\!:$ 20 μ A, $I_{SD}\!\!:$ <1 μ A, MS Package
LT1945	Dual Output, Pos/Neg, 350mA (I _{SW}), Constant Off-Time, High Efficiency Step-Up DC/DC Converter	$V_{IN}\!\!:$ 1.2V to 15V, $V_{OUT(MAX)}\!\!:$ ±34V, $I_{Q}\!\!:$ 20 μ A, $I_{SD}\!\!:$ <1 μ A, MS Package
LT3464	85mA (I _{SW}), High Efficiency Step-Up DC/DC Converter with Integrated Schottky and PNP Disconnect	V _{IN} : 2.3V to 10V, V _{OUT(MAX)} : 34V, I _Q : 25μA, I _{SD} : <1μA, ThinSOT Package

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