

NTQS6463

Power MOSFET 6.8 Amps, 20 Volts

P-Channel TSSOP-8

Features

- New Low Profile TSSOP-8 Package
- Ultra Low $R_{DS(on)}$
- Higher Efficiency Extending Battery Life
- Logic Level Gate Drive
- Diode Exhibits High Speed, Soft Recovery
- Avalanche Energy Specified
- I_{DSS} and $V_{DS(on)}$ Specified at Elevated Temperatures

Applications

- Power Management in Portable and Battery-Powered Products, i.e.: Computers, Printers, PCMCIA Cards, Cellular and Cordless Telephones
- Lithium Ion Battery Applications
- Note Book PC

MAXIMUM RATINGS ($T_C = 25^\circ\text{C}$ unless otherwise noted)

Rating	Symbol	Value	Unit
Drain-to-Source Voltage	V_{DSS}	-20	Vdc
Gate-to-Source Voltage	V_{GS}	± 12	Vdc
Drain Current (Note 1)			Adc
– Continuous @ $T_A = 25^\circ\text{C}$	I_D	5.5	
– Continuous @ $T_A = 70^\circ\text{C}$	I_D	4.4	
– Pulsed (Note 3)	I_{DM}	± 30	
Total Power Dissipation (Note 1) @ $T_A = 25^\circ\text{C}$	P_D	0.93	W
Drain Current (Note 2)			Adc
– Continuous @ $T_A = 25^\circ\text{C}$	I_D	6.8	
– Continuous @ $T_A = 70^\circ\text{C}$	I_D	5.4	
– Pulsed (Note 3)	I_{DM}	± 30	
Total Power Dissipation (Note 2) @ $T_A = 25^\circ\text{C}$	P_D	1.39	W
Operating and Storage Temperature Range	T_J, T_{stg}	-55 to +150	$^\circ\text{C}$
Single Pulse Drain-to-Source Avalanche Energy – Starting $T_J = 25^\circ\text{C}$ ($V_{DD} = 40\text{ V}$, $I_L = 18.4\text{ A}$, $L = 5.0\text{ mH}$, $R_G = 25\ \Omega$)	E_{AS}	845	mJ
Thermal Resistance – Junction-to-Ambient (Note 1) Junction-to-Ambient (Note 2)	$R_{\theta JA}$	134 90	$^\circ\text{C/W}$

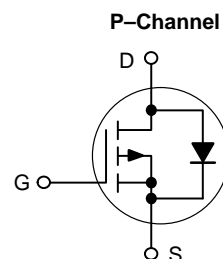
1. Minimum 3" X 3" FR-4 board, steady state.
2. Mounted on 1" square (1 oz.) board, steady state.
3. Pulse Test: Pulse Width = 300 μs , Duty Cycle = 2%.



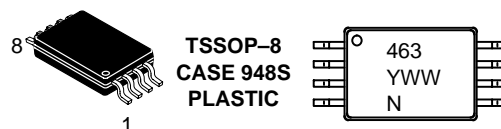
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6.8 AMPERES
20 VOLTS
 $R_{DS(on)} = 20\text{ m}\Omega$

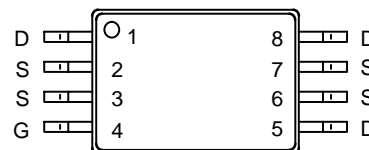


MARKING DIAGRAM



463 = Device Code
Y = Year
WW = Work Week
N = MOSFET

PIN ASSIGNMENT



Top View

ORDERING INFORMATION

Device	Package	Shipping
NTQS6463	TSSOP-8	100 Units/Rail
NTQS6463R2	TSSOP-8	3000/Tape & Reel

NTQS6463

ELECTRICAL CHARACTERISTICS (T_J = 25°C unless otherwise noted)

Characteristic	Symbol	Min	Typ	Max	Unit
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STATIC

Gate Threshold Voltage (V _{DS} = V _{GS} , I _D = -250 μA)	V _{GS(th)}	0.45	0.9	–	Vdc
Gate–Body Leakage (V _{GS} = 0 Vdc, V _{GS} = ±8 Vdc)	I _{GSS}	–	–	±100	nAdc
Zero Gate Threshold Voltage Drain Current (V _{DS} = -16 Vdc, V _{GS} = 0 Vdc) (V _{DS} = -16 Vdc, V _{GS} = 0 Vdc, T _J = 70°C)	I _{DSS}	– –	– –	1.0 10	μAdc
Drain–Source On–State Resistance (Note 4) (V _{GS} = -4.5 Vdc, I _D = -6.8 Adc) (V _{GS} = -2.5 Vdc, I _D = -5.5 Adc)	R _{DS(on)}	– –	0.016 0.022	0.020 0.027	Ω
Forward Transconductance (V _{DS} = -15 Vdc, I _D = -6.8 Adc) (Note 4)	g _{FS}	–	21	–	S
Diode Forward Voltage (I _S = -1.3 Adc, V _{GS} = 0 Vdc) (Note 4)	V _{SD}	–	0.71	1.1	Vdc

DYNAMIC

Total Gate Charge	(V _{DS} = -10 Vdc, V _{GS} = -5.0 Vdc, I _D = -6.8 Adc)	Q _g	–	28	50	nC
Gate–Source Charge		Q _{gs}	–	5.5	–	
Gate–Drain Charge		Q _{gd}	–	9.0	–	
Turn–On Delay Time	(V _{DD} = -10 Vdc, I _D = -1.0 Adc, V _{GS} = -4.5 Vdc, R _G = 6.0 Ω)	t _{d(on)}	–	15	25	ns
Rise Time		t _r	–	22	40	
Turn–Off Delay Time		t _{d(off)}	–	90	150	
Fall Time		t _f	–	53	90	
Source–Drain Reverse Recovery Time	(I _F = -1.3 Adc, di/dt = 100 A/μs)	t _{rr}	–	45	80	ns

4. Pulse Test: Pulse Width ≤ 300 μs, Duty Cycle ≤ 2%.

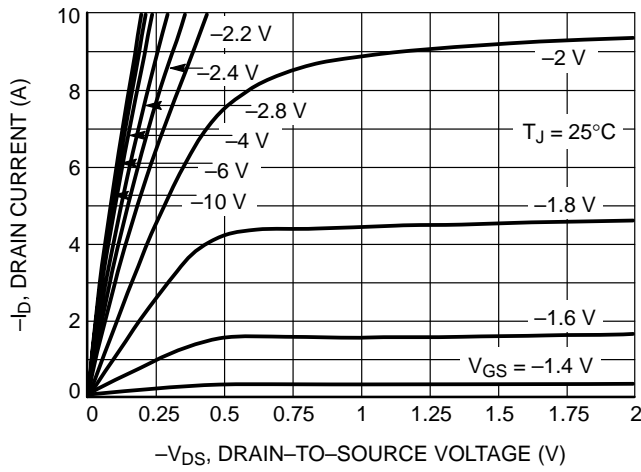


Figure 1. On-Region Characteristics

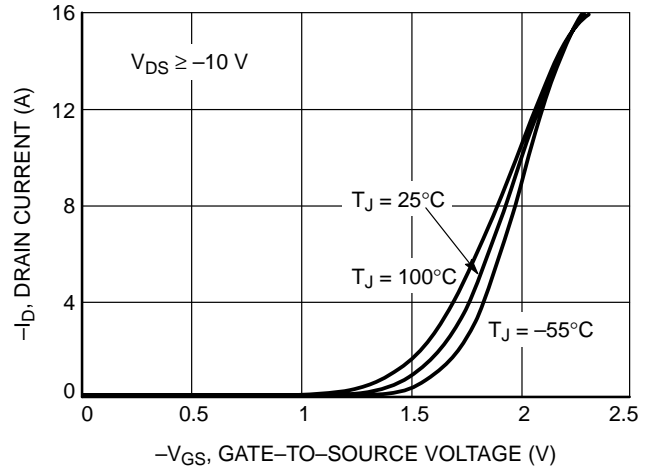


Figure 2. Transfer Characteristics

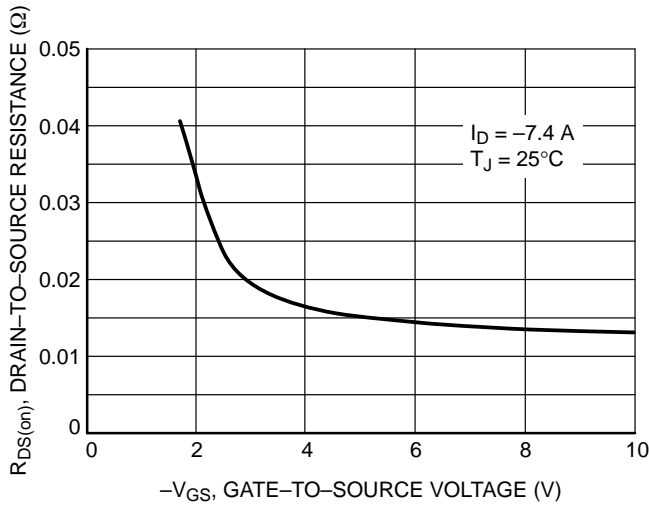


Figure 3. On-Resistance versus Gate-to-Source Voltage

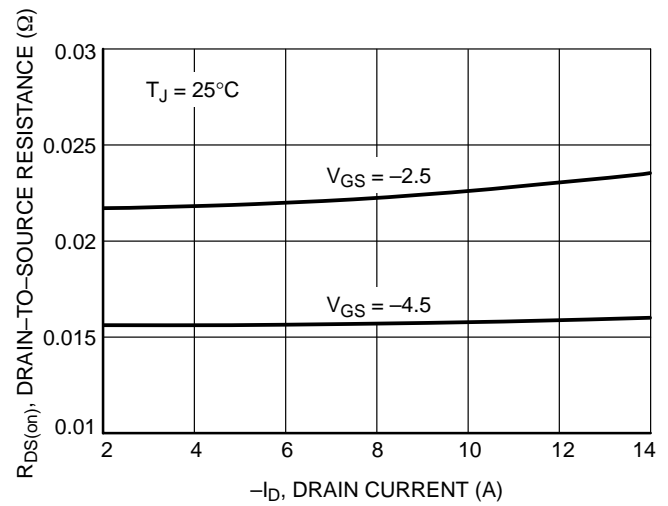


Figure 4. On-Resistance versus Drain Current and Gate Voltage

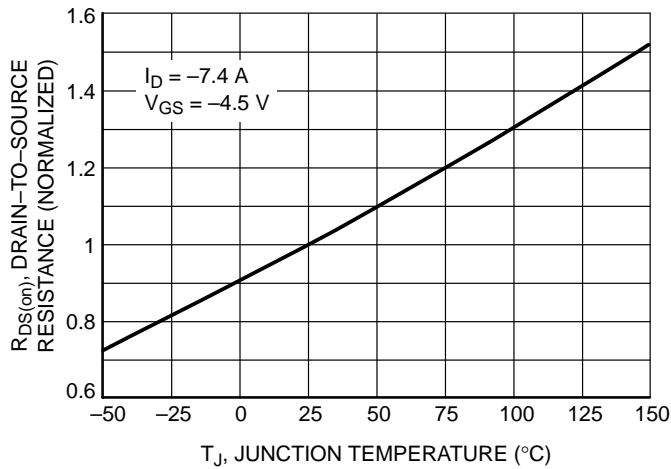


Figure 5. On-Resistance Variation versus Temperature

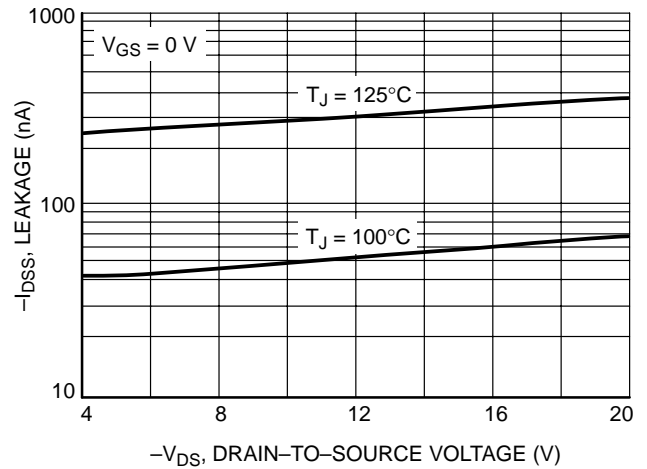


Figure 6. Drain-to-Source Leakage Current versus Voltage

POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (Δt) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ($I_{G(AV)}$) can be made from a rudimentary analysis of the drive circuit so that

$$t = Q/I_{G(AV)}$$

During the rise and fall time interval when switching a resistive load, V_{GS} remains virtually constant at a level known as the plateau voltage, V_{GSP} . Therefore, rise and fall times may be approximated by the following:

$$t_r = Q_2 \times R_G / (V_{GG} - V_{GSP})$$

$$t_f = Q_2 \times R_G / V_{GSP}$$

where

V_{GG} = the gate drive voltage, which varies from zero to V_{GG}

R_G = the gate drive resistance

and Q_2 and V_{GSP} are read from the gate charge curve.

During the turn–on and turn–off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

$$t_{d(on)} = R_G C_{iss} \ln [V_{GG}/(V_{GG} - V_{GSP})]$$

$$t_{d(off)} = R_G C_{iss} \ln (V_{GG}/V_{GSP})$$

The capacitance (C_{iss}) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating $t_{d(on)}$ and is read at a voltage corresponding to the on–state when calculating $t_{d(off)}$.

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by $L di/dt$, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.

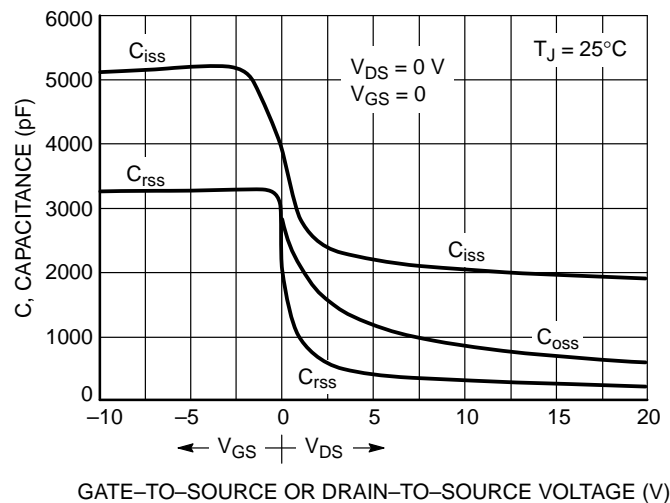


Figure 7. Capacitance Variation

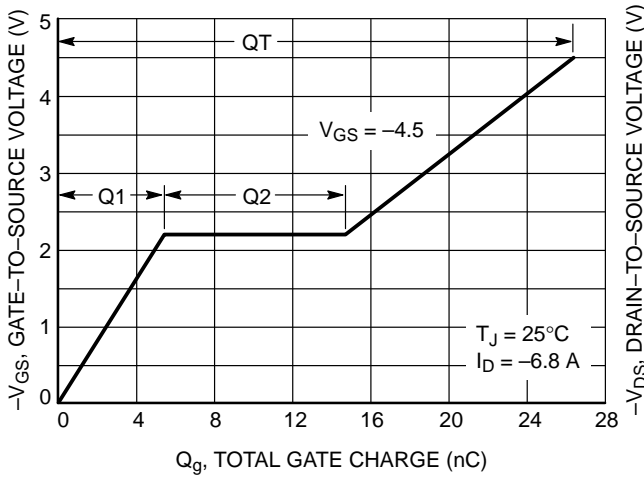


Figure 8. Gate-to-Source and Drain-to-Source Voltage versus Total Charge

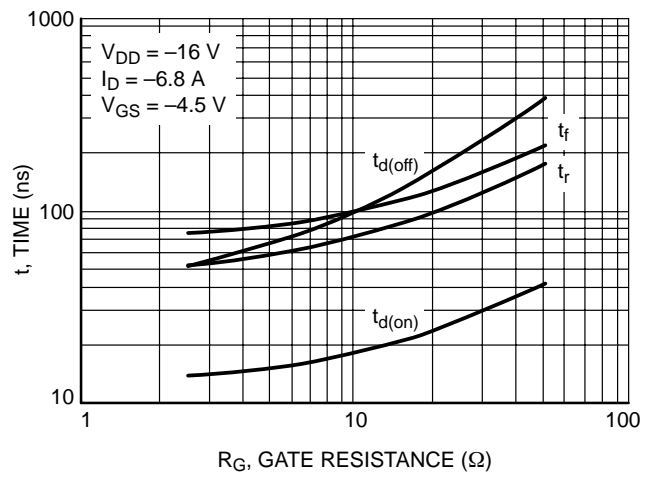


Figure 9. Resistive Switching Time Variation versus Gate Resistance

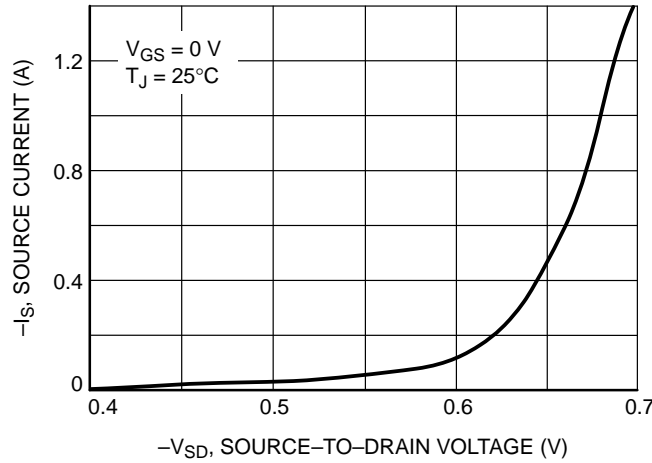


Figure 10. Diode Forward Voltage versus Current

SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain-to-source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (T_C) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, “Transient Thermal Resistance – General Data and Its Use.”

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current (I_{DM}) nor rated voltage (V_{DSS}) is exceeded and the transition time (t_r , t_f) do not exceed 10 μ s. In addition the total power averaged over a complete switching cycle must not exceed $(T_{J(MAX)} - T_C)/(R_{\theta JC})$.

A Power MOSFET designated E-FET can be safely used in switching circuits with unclamped inductive loads. For

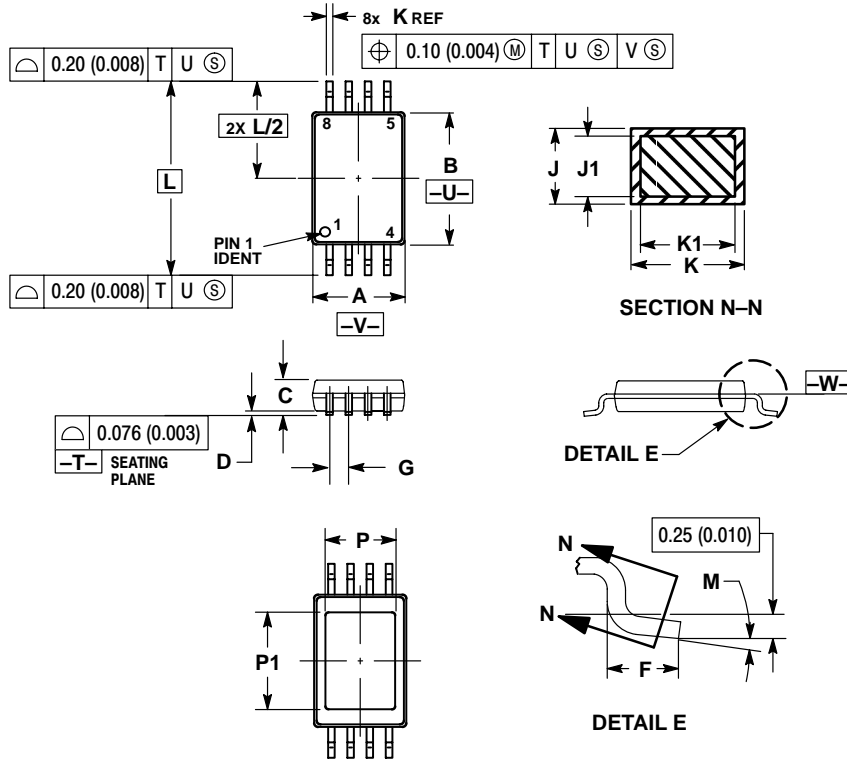
reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non-linearly with an increase of peak current in avalanche and peak junction temperature.

Although many E-FETs can withstand the stress of drain-to-source avalanche at currents up to rated pulsed current (I_{DM}), the energy rating is specified at rated continuous current (I_D), in accordance with industry custom. The energy rating must be derated for temperature. Maximum energy at currents below rated continuous I_D can safely be assumed to equal the values indicated.

NTQS6463

PACKAGE DIMENSIONS

TSSOP-8
CASE 948S-01
ISSUE O




NOTES:

1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
2. CONTROLLING DIMENSION: MILLIMETER.
3. DIMENSION A DOES NOT INCLUDE MOLD FLASH. PROTRUSIONS OR GATE BURRS. MOLD FLASH OR GATE BURRS SHALL NOT EXCEED 0.15 (0.006) PER SIDE.
4. DIMENSION B DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSION. INTERLEAD FLASH OR PROTRUSION SHALL NOT EXCEED 0.25 (0.010) PER SIDE.
5. TERMINAL NUMBERS ARE SHOWN FOR REFERENCE ONLY.
6. DIMENSION A AND B ARE TO BE DETERMINED AT DATUM PLANE -W-.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	2.90	3.10	0.114	0.122
B	4.30	4.50	0.169	0.177
C	---	1.10	---	0.043
D	0.05	0.15	0.002	0.006
F	0.50	0.70	0.020	0.028
G	0.65 BSC		0.026 BSC	
J	0.09	0.20	0.004	0.008
J1	0.09	0.16	0.004	0.006
K	0.19	0.30	0.007	0.012
K1	0.19	0.25	0.007	0.010
L	6.40 BSC		0.252 BSC	
M	0°	8°	0°	8°
P	---	2.20	---	0.087
P1	---	3.20	---	0.126

Notes

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