

Low-Current Superhet Remote Control Receiver

Description

The U4311B is a monolithic integrated circuit in bipolar technology for low-current UHF remote control superheterodyne receivers in amplitude- or frequency-modulated mode. Typical applications are keyless car

lock-, alarm- or tele-control remote indication systems. Especially for automotive applications, it supports a superhet design with about 1 mA total current consumption as required by the car manufacturers.

Features

- Usable for amplitude- and frequency-modulated transmission systems
- Extremely low quiescent current (approximately 1 mA in standby mode due to wake-up concept)
- Wide power supply voltage range 3 to 13 V
- Sensitive IF amplifier for 10.7-MHz operating frequency
- Logarithmic AM demodulator
- FM demodulator
- Monoflop exit to wake up a microcontroller
- High-performance operational amplifier to realize a data recovering filter
- Non-inverting clamping comparator with amplitudedepending hysteresis for data regeneration

Block Diagram

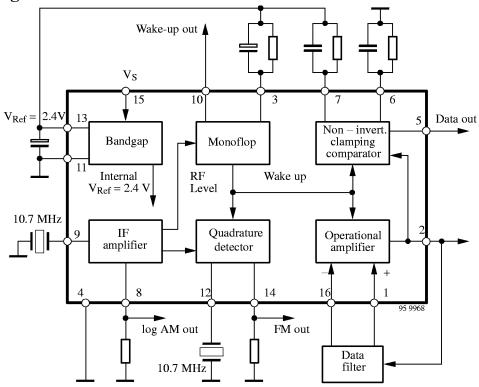


Figure 1. Block diagram

Ordering Information

-		
Extended Type Number	Package	Remarks
U4311B-C	DIP16	
U4311B-CFL	SO16L	



Pin Description

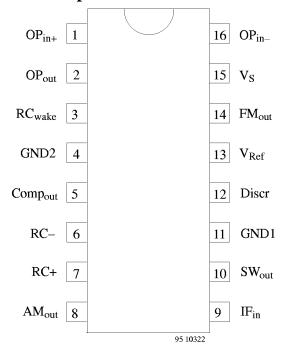


Figure 2. Pin description

Pin	Symbol	Function
1	OP _{in+}	OP amplifier non-inverted input
2	OP _{out}	OP amplifier output
3	RC _{wake}	RC wake-up reset time
4	GND2	Ground of the logical circuits
5	Compout	Comparator output
6	RC-	Comparator time constant
7	RC+	Comparator time constant
8	AM _{out}	AM current output
9	IF _{in}	IF input
10	SW _{out}	Wake-up output
11	GND1	Ground of the analog circuits
12	Discr	FM discriminator tank
13	$V_{ m Ref}$	Reference voltage
14	FM _{out}	FM discriminator output
15	V_S	Supply voltage
16	OP_{in-}	OP amplifier inverted input

Internal connections see figures 4 to 19

Absolute Maximum Ratings

Parameters	Symbol	Value	Unit
Supply voltage	V_{S}	13	V
Power dissipation $T_{amb} = 85^{\circ}C$	P _{tot}	400	mW
Junction temperature	T_{j}	125	°C
Ambient temperature	T_{amb}	-40 to +85	°C
Storage temperature	T _{sto}	-55 to +125	°C

Thermal Resistance

	Parameters	Symbol	Value	Unit
Junction ambient	DIP16	R _{thJA}	120	K/W
	SO16L	R_{thJA}	100	K/W



Electrical Characteristics

 $V_S = 5 \ \text{V}, \ T_{amb} = 25 \text{°C}, \ f_{in} = 10.7 \ \text{MHz}; \ \text{FM part:} \ f_{mod} = 1 \ \text{kHz}, \ f_{dev} = 22.5 \ \text{kHz}; \ \text{AM part:} \ f_{mod} = 1 \ \text{kHz}, \ m = 100\% \ \text{unless otherwise specified}$

Parameters	Test Co	nditions / Pins	Symbol	Min.	Тур.	Max.	Unit
Characteristics			-			***************************************	.,
Supply-voltage range		Pin 15	V_{S}	3		12	V
Quiescent supply current		Pin 15	I_q		1	1.3	mA
Active supply current		Pin 15	I _{act}		2.8	3.6	mA
Bandgap	1						1
Regulated voltage		Pin 13	V _{Ref}	2.3	2.4	2.5	V
Output current		Pin 13	I_{Ref}			5	mA
Source resistance		Pin 13	R _{Ref}		2.3	5	Ω
External capacitor		Pin 13	C _{Ref}	10			μF
Power-supply rejection	f = 50 Hz	Pin 13	psrr		60		dB
ratio			_				
IF amplifier							
Input resistance		Pin 9	R _{in}	180	330	520	Ω
Input capacitance		Pin 9	Cin		5		pF
Typical internal 3 dB	IF level 70	dΒμV	f_{3dB}	8		12	MHz
frequency		Pins 9 and 14					
−3 dB limiting point		Pin 9	V_{FM3dB}		30		dΒμV
Recovered data voltage		Pin 14	V _{FMout}	50	130	230	mV
FM detector output		Pin 14	R _{FMout}		50		kΩ
resistance							
AM rejection ratio	m = 30%	Pins 9 and 14	AM_{rr}		25		dB
Maximum AM input voltage		Pin 9	V _{AMmax}		90		dΒμV
AM quiescent current		Pin 8	I _{AMout}	10	22	37	μA
Maximum AM current		Pin 8	I _{AMoutmax}		100		μA
Operational amplifier							
Gain-bandwidth product		Pins 1, 2 and 16	f _t	3	4	6.5	MHz
Excess phase		Pins 1, 2 and 16	δ		80		degree
Open loop gain		Pins 1, 2 and 16	g_0	50	70	95	dB
Output voltage range		Pin 2	$\Delta V_{ m out}$		1.55		V
Common-mode input voltage		Pins 1 and 16	V _{in}	0.7		1.7	V
Input offset voltage		Pins 1 and 16	Vos	-2.5	0	+2.5	mV
Maximum output current		Pin 2	I _{out}			5	mA
Common-mode rejection		Pin 1 and 16	cmrr	65	85		dB
ratio							
Total harmonic distortion	V _{in} < 300 unity gain	mV, f = 33 kHz, circuit Pin 2	thd		1	3	%
Power-supply rejection ratio	f = 50 Hz	Pin 2	psrr	65	85		dB

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Parameters	Test Conditions / Pins	Symbol	Min.	Тур.	Max.	Unit			
Clamping comparator									
Typical common-mode input voltage range			0.8		1.6	V			
Maximum distortion voltage	$\begin{aligned} &V_{signal} = 100 \text{ mV}, \\ &R+=R-=50 \text{ k}\Omega, \\ &C+=C-=200 \text{ nF}, \\ &f_{disto} = 50 \text{ Hz}, \\ &f_{signal} = 1 \text{ kHz} \end{aligned}$	$ m V_{dmax}$			200	mV			
Output voltage	$\begin{aligned} V_2 > (V_6 + V_7) /2 \\ (10-k\Omega \text{ load to } V_{\text{Ref}}) \\ &\text{Pin 5} \end{aligned}$	V _{cout}		V_{Ref}		V			
Output voltage	$ \begin{array}{c} V_2 < (V_6 + V_7)/2 \\ (10-k\Omega \text{ load to } V_{Ref}) \\ \text{Pin 5} \end{array} $	V_{cout}	0	150	250	mV			
Wake-up circuit									
Minimum wake-up level	Pin 9	V _{in}		40		dBµV 1)			
Internal charging resistor	Pin 3	Rint		1.5		kΩ			
Threshold voltage	Pin 3	V _{th}		1.6		V			
Output switch current	Pin 10	I_{SW}	180	250	550	μA			
Output switch voltage	Pin 10	V_{SW}			5.5	V 2)			
External wake-up resistor	Pins 3 and 13	R _{WU}	22			kΩ			
External wake-up capacitor	Pins 3 and 13	$C_{ m WU}$			10	μF			
Hold time (± 30%)		t _h	$\approx 1.5 \times R_{WU} \times C_{WU}$			s 3)			
Delay time (± 30%)		t _d	$\approx C_{\mathrm{WU}} \times 0.75 \mathrm{~k}\Omega$			s 3)			

- 1) Measured at Pin 9, referred to 330 Ω
- 2) Protected by a Z-diode, see figure 13
- 3) Valid for 0.1 $\mu F \le C_{WU} \le 10~\mu F$ and 22 $k\Omega \le R_{WU} \le 680~k\Omega$

Circuit Description

General Functions

The integrated circuit U4311B includes the following functions: IF amplifier, FM demodulator, wake-up circuit with monoflop, operational amplifier, non-inverting data comparator and voltage regulator.

The 10.7-MHz IF signal from the front end passes the integrated IF-amplifier which operates for amplitude- or frequency-modulated signals to either a logarithmic AM demodulator which was implemented to avoid settling-time problems effected by use of an automatic gain control system or a quadrature detector for FM. A data-shaping filter — advantageously realized with the internal high-performance operational amplifier — reduces system bandwidth to an optimized compromise regarding transmission distance and data recognition. Thus, an optimal bit-error rate can be achieved without any further active component.

The comparator connected to the output of the filter has a level-dependent hysteresis and clamps its reference voltage to the signal's minimum and maximum peaks as described later.

Without IF-input signal — in normal mode — only the IF amplifier and the AM demodulator which operates as a

level-strength indicator are activated. If the level of the IF signal increases, the entire circuitry is turned on by the wake-up circuit. This signal is externally available at Pin 10 and can be used to wake up a microcontroller. After an adjustable reset time, determined by the monoflop time constant, the integrated circuit returns to sleep mode. In this case, typically 1-mA supply current is required. An external resistor matched at Pin 3 to ground blocks the wake-up circuit and enables the complete functionality at lower IF levels as can be seen in figures 24 and 27, but supply current increases up to typically 2.8 mA.

Function of the Clamping Comparator

The output signal of the operational amplifier is fed to the input of the non-inverting comparator and two peak detectors (Q1 and Q2, figure 3). Their time constants are distinguished by RC+ and RC-. The component's value must be adapted to the transmission code. The time constant should be large compared to the bit rate for optimized noise and hum suppression. To compensate the input transistor's base-emitter-voltage differences, these two signals are buffered by Q3 and Q4. The mean value is used as comparator threshold, the difference of the peak values controls the hysteresis. This clamping comparator operates as a data regenerator.

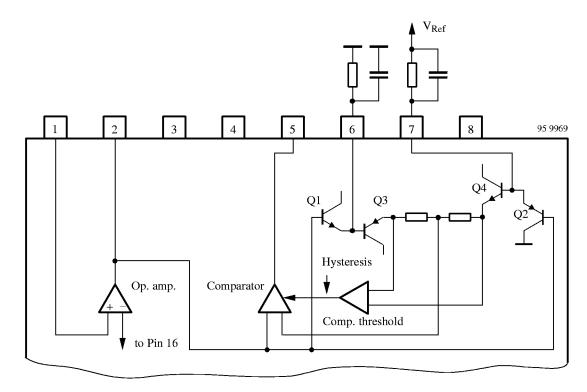


Figure 3. Principle function of the clamping comparator

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Internal Pin Circuitry

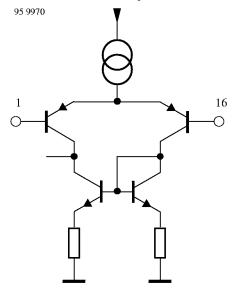


Figure 4. Pin 1 OP_{in+}

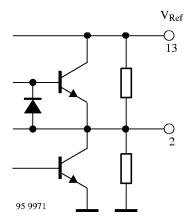


Figure 5. Pin 2 OP_{out}

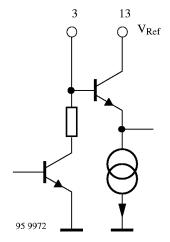


Figure 6. Pin 3 RC_{wake}



Figure 7. Pin 4 GND2

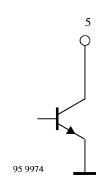


Figure 8. Pin 5 Compout

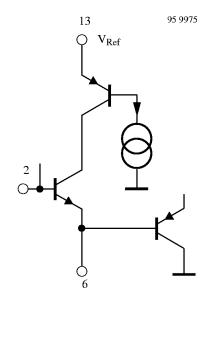


Figure 9. Pin 6 RC-

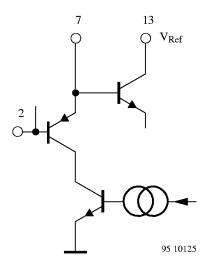


Figure 10. Pin 7 RC+

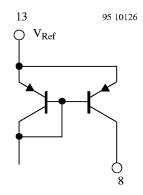


Figure 11. Pin 8 AM_{out}

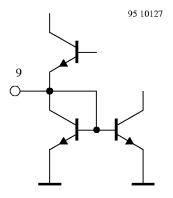


Figure 12. Pin 9 IF_{in}

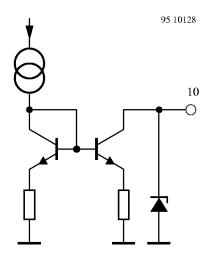


Figure 13. Pin 10 SW_{out}



Figure 14. Pin 11 GND1

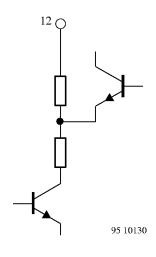


Figure 15. Pin 12 Discr

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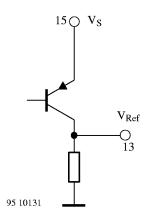


Figure 16. Pin 13 V_{Ref}

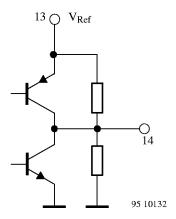


Figure 17. Pin 14 FM_{out}



Figure 18. Pin 15 V_S

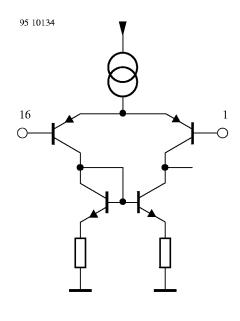


Figure 19. Pin 16 OP_{in}

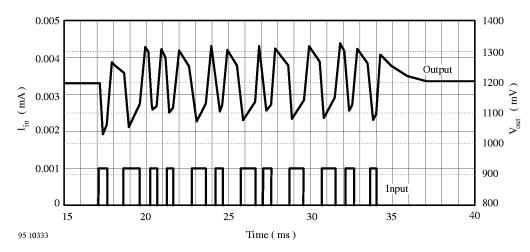


Figure 20. Time domain response of 2-kHz Bessel lowpass data filter

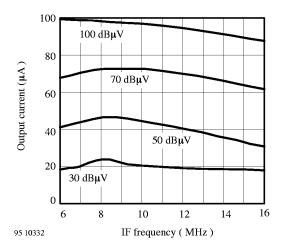


Figure 21. IF-frequency response

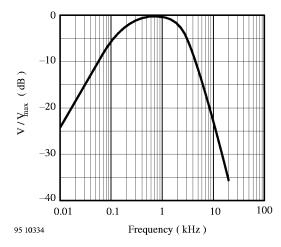


Figure 22. Frequency response of 2-kHz Bessel lowpass data filter

Data-Recovering Filter

The test circuit in figures 23 and 26 includes an example of a data-recovering filter realized with the components R_1, R_2, C_1, C_2, C_3 . It is of a second-order Bessel type with lowpass characteristic, a 3-dB cut-off frequency of 2 kHz and an additional highpass characteristic for suppressing dc and low-frequency ac components. Simulation of time domain and frequency response can be seen in figures 20 and 22. This filter gives a typical application of a 1-kBaud Manchester-code, amplitude-modulated transmission.

The capacitor C_2 is responsible for the highpass cut-off frequency. In order to achieve a correct pulse response, this highpass cut-off frequency should be as low as possible. Figure 20 shows the transient response and the influence of the dc component. The first pulses might be wrong if the highpass cut-off frequency is too low. For this reason, some burst bits must be transmitted before the real data transmission starts. On the other hand, if the cut-off frequency is too high, roof shaping of the rectangle pulses at the operational amplifier output might causes problems.

The lowpass cut-off frequency and the maximum transimpedance V_{out}/I_{in} are distinguished by the further external elements. Careful design of the data filter enables optimized transmission range. For designing other filter parameters, please refer to filter design handbooks/ programs or request TEMIC for support. Some proposals can be found in the application notes ANT012, ANT013 and ANT015.



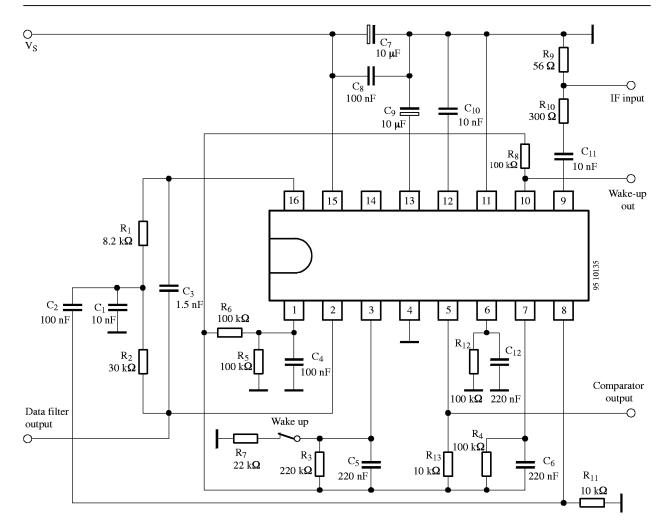


Figure 23. AM test circuit with 2-kHz Bessel lowpass data filter

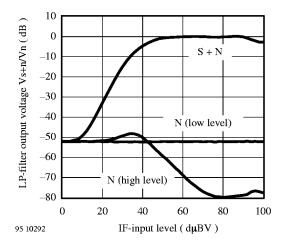


Figure 24. Signal-to-noise ratio AM

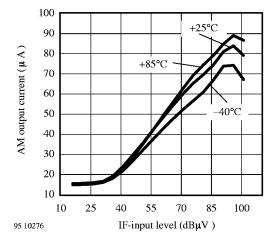


Figure 25. AM-demodulator characteristic vs. temperature

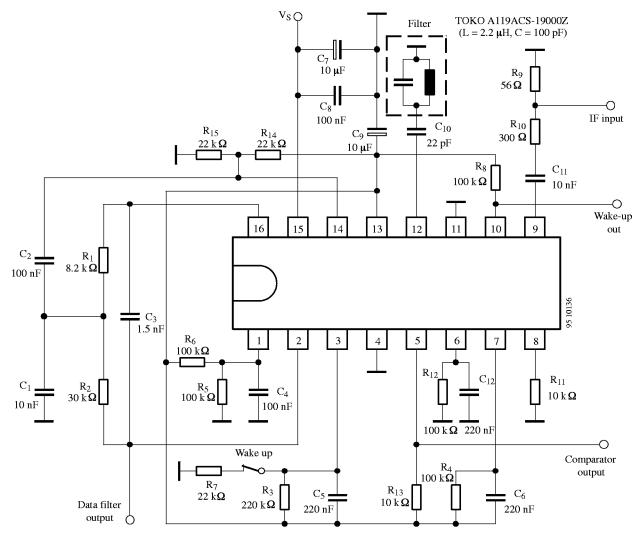
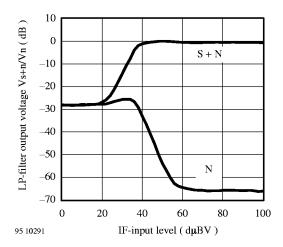
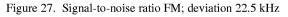


Figure 26. FM test circuit with 2-kHz Bessel lowpass data filter





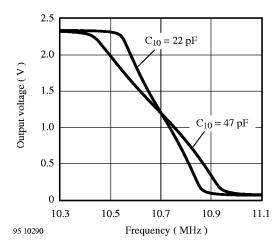


Figure 28. FM-discriminator characteristic



Application

The U4311B is well-suited to implement UHF remote control or data transmission systems, based on a low-current superheterodyne receiver concept. SAW-devices may be used in the transmitter's as well as in the receiver local oscillator. The front end should be a discrete circuit application with low-current UHF transistors such as S822T or S852T (Vishay Telefunken). The frequency of the local oscillator can be determined either by coaxial resonators or SAW devices. Due to large SAW-resonator tolerance, an IF bandwidth — and in a

FM system additionally the discriminator amplitude characteristic (figure 28) — of 300 kHz or higher is proposed. As the circuit needs only 3.0 V supply voltage for operation, the front end may be a stacked design in order to achieve a total receiver current consumption of approximately 1 mA. Figure 29 shows a principle receiver concept diagram. The application notes ANT012, ANT013, and ANT015 contain more detailed information on complete RF links.

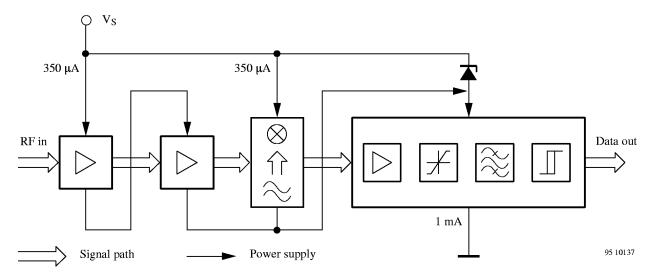
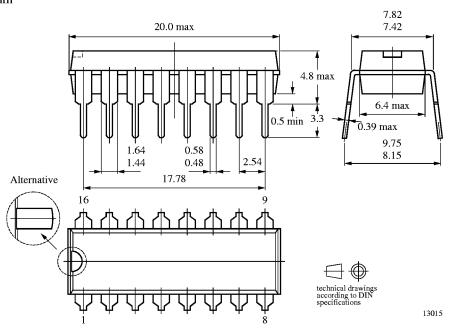


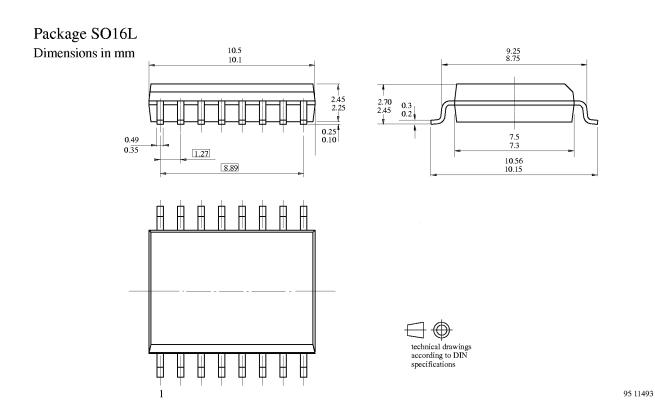
Figure 29. Principle diagram of a UHF remote control receiver



Package Information

Package DIP16 Dimensions in mm







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It is the policy of **TEMIC Semiconductor GmbH** to

- 1. Meet all present and future national and international statutory requirements.
- 2. Regularly and continuously improve the performance of our products, processes, distribution and operating systems with respect to their impact on the health and safety of our employees and the public, as well as their impact on the environment.

It is particular concern to control or eliminate releases of those substances into the atmosphere which are known as ozone depleting substances (ODSs).

The Montreal Protocol (1987) and its London Amendments (1990) intend to severely restrict the use of ODSs and forbid their use within the next ten years. Various national and international initiatives are pressing for an earlier ban on these substances.

TEMIC Semiconductor GmbH has been able to use its policy of continuous improvements to eliminate the use of ODSs listed in the following documents.

- 1. Annex A, B and list of transitional substances of the Montreal Protocol and the London Amendments respectively
- 2. Class I and II ozone depleting substances in the Clean Air Act Amendments of 1990 by the Environmental Protection Agency (EPA) in the USA
- 3. Council Decision 88/540/EEC and 91/690/EEC Annex A, B and C (transitional substances) respectively.

TEMIC Semiconductor GmbH can certify that our semiconductors are not manufactured with ozone depleting substances and do not contain such substances.

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