

## 1500 Watt MOSORB

**GENERAL DATA APPLICABLE TO ALL SERIES IN THIS GROUP**

### Zener Transient Voltage Suppressors Unidirectional and Bidirectional

Mosorb devices are designed to protect voltage sensitive components from high voltage, high energy transients. They have excellent clamping capability, high surge capability, low zener impedance and fast response time. These devices are Motorola's exclusive, cost-effective, highly reliable Surmetic axial leaded package and are ideally-suited for use in communication systems, numerical controls, process controls, medical equipment, business machines, power supplies and many other industrial/consumer applications, to protect CMOS, MOS and Bipolar integrated circuits.

**Specification Features:**

- Standard Voltage Range — 6.2 to 250 V
- Peak Power — 1500 Watts @ 1 ms
- Maximum Clamp Voltage @ Peak Pulse Current
- Low Leakage < 5  $\mu$ A Above 10 V
- UL Recognition
- Response Time is Typically < 1 ns

**Mechanical Characteristics:**

**CASE:** Void-free, transfer-molded, thermosetting plastic

**FINISH:** All external surfaces are corrosion resistant and leads are readily solderable

**POLARITY:** Cathode indicated by polarity band. When operated in zener mode, will be positive with respect to anode

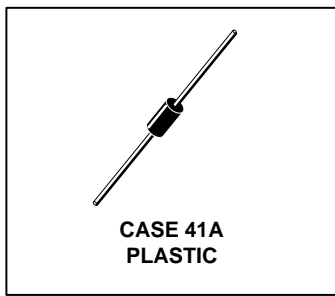
**MOUNTING POSITION:** Any

**WAFER FAB LOCATION:** Phoenix, Arizona

**ASSEMBLY/TEST LOCATION:** Guadalajara, Mexico

**1N6373A  
SERIES  
1500 WATT  
PEAK POWER**

**MOSORB  
ZENER OVERVOLTAGE  
TRANSIENT  
SUPPRESSORS  
6.2-250 VOLTS  
1500 WATT PEAK POWER  
5 WATTS STEADY STATE**



**MAXIMUM RATINGS**

Rating	Symbol	Value	Unit
Peak Power Dissipation (1) @ $T_L \leq 25^\circ\text{C}$	P <sub>PK</sub>	1500	Watts
Steady State Power Dissipation @ $T_L \leq 75^\circ\text{C}$ , Lead Length = 3/8" Derated above $T_L = 75^\circ\text{C}$	P <sub>D</sub>	5	Watts
		50	mW/°C
Forward Surge Current (2) @ $T_A = 25^\circ\text{C}$	I <sub>FSM</sub>	200	Amps
Operating and Storage Temperature Range	T <sub>J</sub> , T <sub>stg</sub>	- 65 to +175	°C

Lead temperature not less than 1/16" from the case for 10 seconds: 230°C

NOTES: 1. Nonrepetitive current pulse per Figure 5 and derated above  $T_A = 25^\circ\text{C}$  per Figure 2.  
2. 1/2 sine wave (or equivalent square wave), PW = 8.3 ms, duty cycle = 4 pulses per minute maximum.

Devices listed in bold, italic are Motorola preferred devices.

**\*ELECTRICAL CHARACTERISTICS** ( $T_A = 25^\circ\text{C}$  unless otherwise noted)  $V_F\# = 3.5\text{ V Max}$ ,  $I_F^{**} = 100\text{ A}$  (C suffix denotes standard back to back bidirectional versions. Test both polarities)

JEDEC Device Note 1	Device Note 1	Breakdown <sup>††</sup> Voltage		Maximum Reverse Stand-Off Voltage $V_{RWM}^{***}$ (Volts)	Maximum Reverse Leakage $I_R$ ( $\mu\text{A}$ ) @ $V_{RWM}$	Maximum Reverse Surge Current $I_{RSM}^\dagger$ (Amps)	Maximum Reverse Voltage @ $I_{RSM}^\dagger$ (Clamping Voltage) $V_{RSM}$ (Volts)	Clamping Voltage	
		$V_{BR}$ Volts Min	@ $I_T$ (mA)					Peak Pulse Current @ $I_{pp1}^\dagger = 1\text{ A}$ $V_{C1}$ (Volts max)	Peak Pulse Current @ $I_{pp1}^\dagger = 10\text{ A}$ $V_{C2}$ (Volts max)
<b>1N6373</b>	<b>ICTE-5/MPTE-5</b>	<b>6</b>	<b>1</b>	<b>5</b>	<b>300</b>	<b>160</b>	<b>9.4</b>	<b>7.1</b>	<b>7.5</b>
1N6374	ICTE-8/MPTE-8	9.4	1	8	25	100	15	11.3	11.5
1N6382	ICTE-8C/MPTE-8C	9.4	1	8	25	100	15	11.4	11.6
1N6375	ICTE-10/MPTE-10	11.7	1	10	2	90	16.7	13.7	14.1
1N6383	ICTE-10C/MPTE-10C	11.7	1	10	2	90	16.7	14.1	14.5
1N6376	ICTE-12/MPTE-12	14.1	1	12	2	70	21.2	16.1	16.5
1N6384	ICTE-12C/MPTE-12C	14.1	1	12	2	70	21.2	16.7	17.1
1N6377	ICTE-15/MPTE-15	17.6	1	15	2	60	25	20.1	20.6
1N6385	ICTE-15C/MPTE-15C	17.6	1	15	2	60	25	20.8	21.4
1N6378	ICTE-18/MPTE-18	21.2	1	18	2	50	30	24.2	25.2
1N6386	ICTE-18C/MPTE-18C	21.2	1	18	2	50	30	24.8	25.5
1N6379	ICTE-22/MPTE-22	25.9	1	22	2	40	37.5	29.8	32
1N6387	ICTE-22C/MPTE-22C	25.9	1	22	2	40	37.5	30.8	32
1N6380	ICTE-36/MPTE-36	42.4	1	36	2	23	65.2	50.6	54.3
1N6388	ICTE-36C/MPTE-36C	42.4	1	36	2	23	65.2	50.6	54.3
1N6381	ICTE-45/MPTE-45	52.9	1	45	2	19	78.9	63.3	70
1N6389	ICTE-45C/MPTE-45C	52.9	1	45	2	19	78.9	63.3	70

NOTE 1: C suffix denotes standard back-to-back bidirectional versions. Test both polarities. JEDEC device types 1N6382 thru 1N6389 are registered as back to back bidirectional versions and do not require a C suffix. 1N6373 thru 1N6381 are registered as unidirectional devices only (no bidirectional option).

\* Indicates JEDEC registered data.

\*\* 1/2 sine wave (or equivalent square wave),  $PW = 8.3\text{ ms}$ , duty cycle = 4 pulses per minute maximum.

\*\*\* A transient suppressor is normally selected according to the maximum reverse stand-off voltage ( $V_{RWM}$ ), which should be equal to or greater than the dc or continuous peak operating voltage level.

† Surge current waveform per Figure 5 and derate per Figure 2 of the General Data — 1500 W at the beginning of this group.

††  $V_{BR}$  measured at pulse test current  $I_T$  at an ambient temperature of  $25^\circ\text{C}$ .

#  $V_F$  applies to unidirectional devices only.

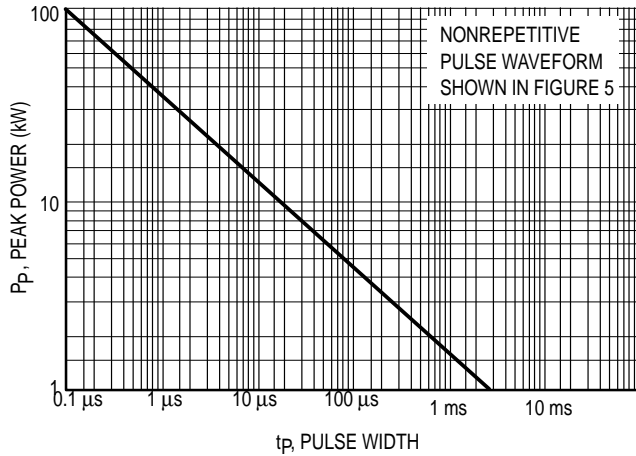


Figure 1. Pulse Rating Curve

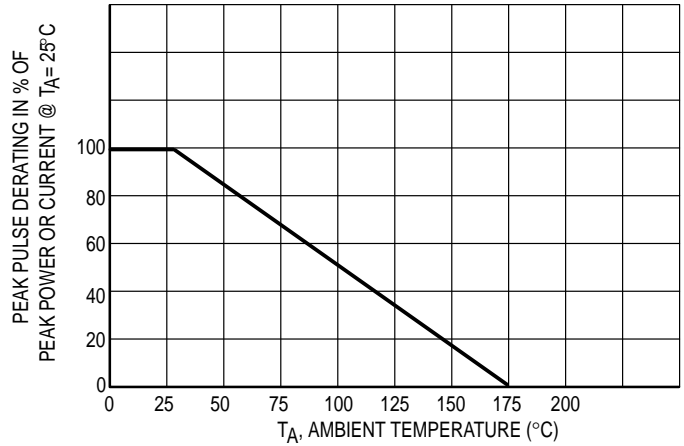
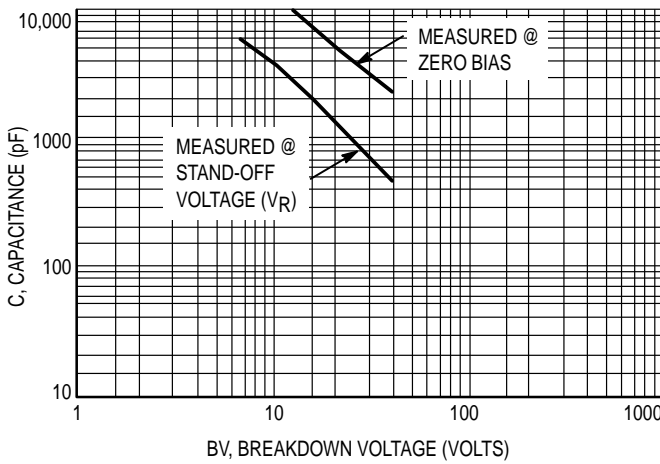


Figure 2. Pulse Derating Curve

**1N6373, ICTE-5, MPTE-5,**  
through  
**1N6389, ICTE-45, C, MPTE-45, C**



**1N6267A/1.5KE6.8A**  
through  
**1N6303A/1.5KE200A**

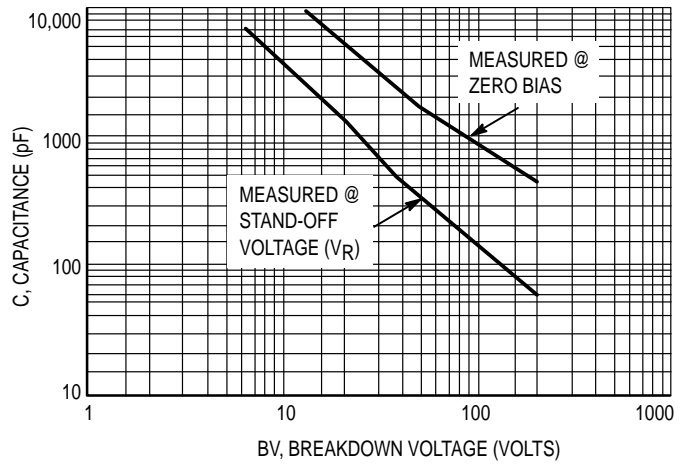


Figure 3. Capacitance versus Breakdown Voltage

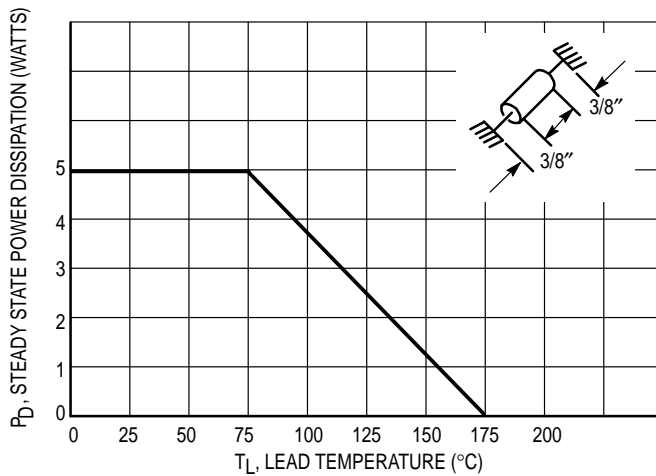


Figure 4. Steady State Power Derating

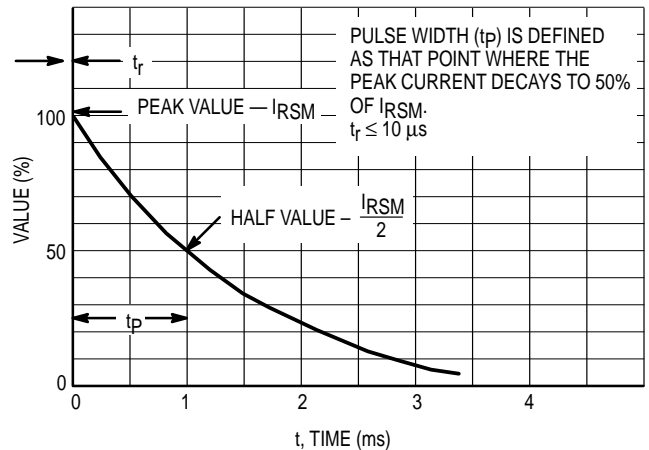
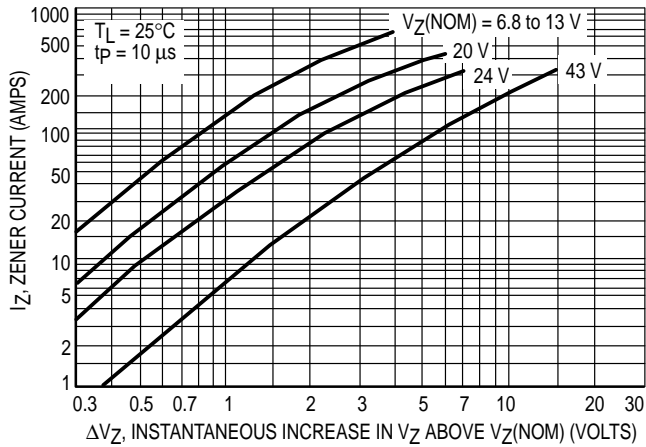


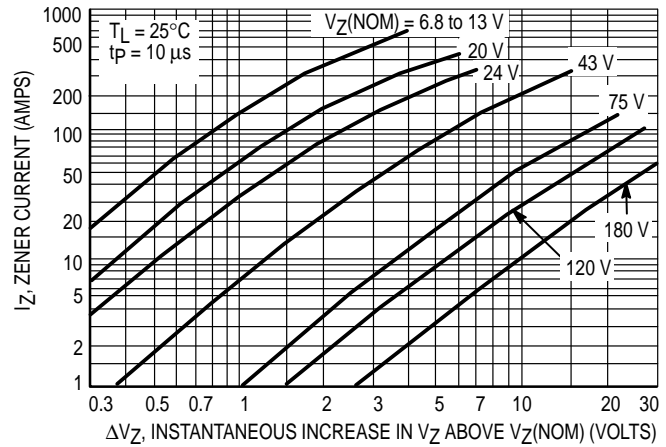
Figure 5. Pulse Waveform

Devices listed in bold, italic are Motorola preferred devices.

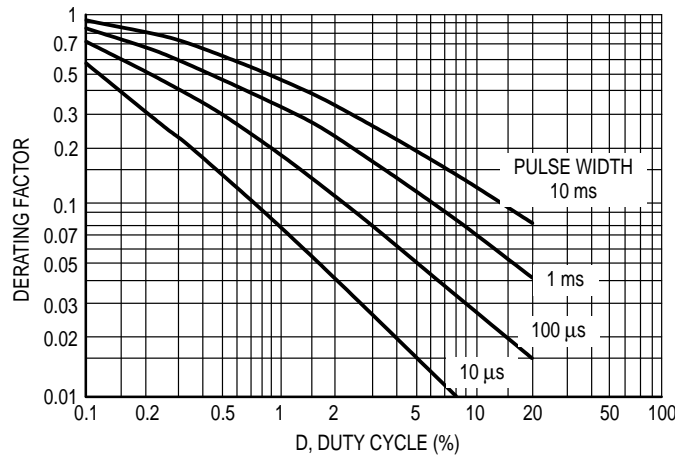
**1N6373, ICTE-5, MPTE-5,  
through  
1N6389, ICTE-45, C, MPTE-45, C**



**1N6267A/1.5KE6.8A  
through  
1N6303A/1.5KE200A**



**Figure 6. Dynamic Impedance**



**Figure 7. Typical Derating Factor for Duty Cycle**

**APPLICATION NOTES**

**RESPONSE TIME**

In most applications, the transient suppressor device is placed in parallel with the equipment or component to be protected. In this situation, there is a time delay associated with the capacitance of the device and an overshoot condition associated with the inductance of the device and the inductance of the connection method. The capacitance effect is of minor importance in the parallel protection scheme because it only produces a time delay in the transition from the operating voltage to the clamp voltage as shown in Figure A.

The inductive effects in the device are due to actual turn-on time (time required for the device to go from zero current to full current) and lead inductance. This inductive effect produces an overshoot in the voltage across the equipment or component being protected as shown in Figure B. Minimizing this overshoot is very important in the application, since the main purpose for adding a transient suppressor is to clamp voltage spikes. These devices have excellent response time, typically in the picosecond range and negligible inductance. However, external inductive effects could produce unacceptable overshoot. Proper circuit layout, minimum lead lengths

and placing the suppressor device as close as possible to the equipment or components to be protected will minimize this overshoot.

Some input impedance represented by  $Z_{in}$  is essential to prevent overstress of the protection device. This impedance should be as high as possible, without restricting the circuit operation.

**DUTY CYCLE DERATING**

The data of Figure 1 applies for non-repetitive conditions and at a lead temperature of  $25^\circ\text{C}$ . If the duty cycle increases, the peak power must be reduced as indicated by the curves of Figure 7. Average power must be derated as the lead or ambient temperature rises above  $25^\circ\text{C}$ . The average power derating curve normally given on data sheets may be normalized and used for this purpose.

At first glance the derating curves of Figure 7 appear to be in error as the 10 ms pulse has a higher derating factor than the 10  $\mu\text{s}$  pulse. However, when the derating factor for a given pulse of Figure 7 is multiplied by the peak power value of Figure 1 for the same pulse, the results follow the expected trend.

## TYPICAL PROTECTION CIRCUIT

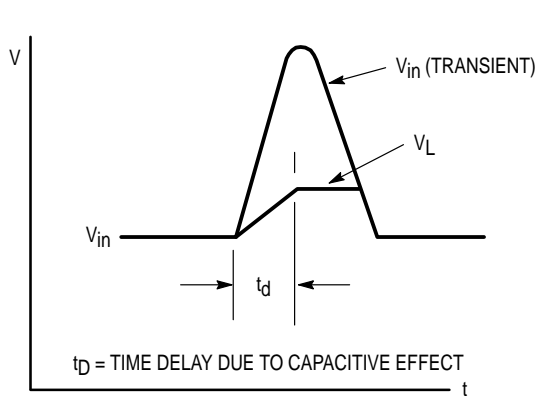
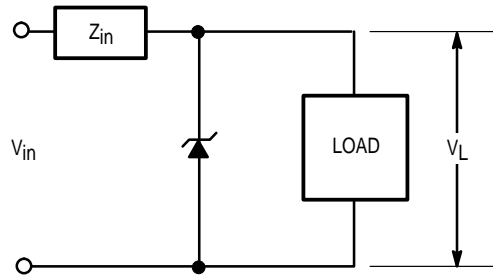


Figure 8.

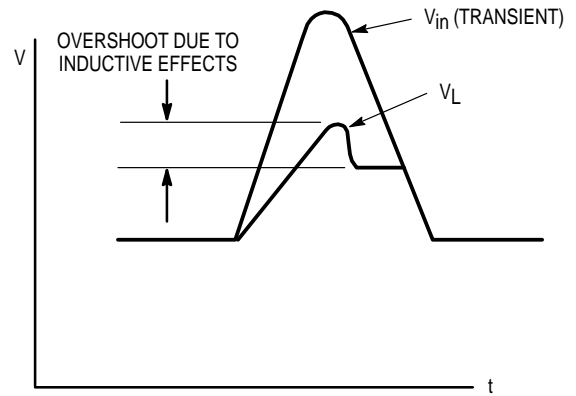


Figure 9.

## UL RECOGNITION\*

The entire series has *Underwriters Laboratory Recognition* for the classification of protectors (QVGV2) under the UL standard for safety 497B and File #116110. Many competitors only have one or two devices recognized or have recognition in a non-protective category. Some competitors have no recognition at all. With the UL497B recognition, our parts successfully passed several tests including Strike Voltage Breakdown test, Endurance Conditioning, Temperature test,

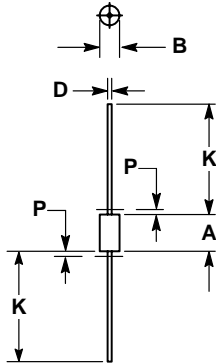
Dielectric Voltage-Withstand test, Discharge test and several more.

Whereas, some competitors have only passed a flammability test for the package material, we have been recognized for much more to be included in their Protector category.

\*Applies to 1.5KE6.8A, CA thru 1.5KE250A, CA

# Transient Voltage Suppressors — Axial Leaded

## 1500 Watt Peak Power



- NOTES:
1. DIMENSIONING AND TOLERANCING PER ANSI Y14.5M, 1982.
  2. CONTROLLING DIMENSION: INCH.
  3. LEAD FINISH AND DIAMETER UNCONTROLLED IN DIM P.

DIM	INCHES		MILLIMETERS	
	MIN	MAX	MIN	MAX
A	0.360	0.375	9.14	9.52
B	0.190	0.205	4.83	5.21
D	0.038	0.042	0.97	1.07
K	1.000	—	25.40	—
P	—	0.050	—	1.27

**CASE 41A-02  
PLASTIC**

(Refer to Section 10 for Surface Mount, Thermal Data and Footprint Information.)

### MULTIPLE PACKAGE QUANTITY (MPQ) REQUIREMENTS

Package Option	Type No. Suffix	MPQ (Units)
Tape and Reel	RL4	1.5K

(Refer to Section 10 for more information on Packaging Specifications.)