## HIGH VOLTAGE FAST-SWITCHING NPN POWER TRANSISTOR

- STMicroelectronics PREFERRED SALESTYPE
- HIGH VOLTAGE CAPABILITY
- VERY HIGH SWITCHING SPEED
- U.L. RECOGNISED ISOWATT218 PACKAGE (U.L. FILE \# E81734 (N))


## APPLICATIONS:

- HORIZONTAL DEFLECTION FOR MONITORS


## DESCRIPTION

The THD200FI is manufactured using Multiepitaxial Mesa technology for cost-effective high performance and uses a Hollow Emitter structure to enhance switching speeds.
The THD series is designed for use in horizontal deflection circuits in televisions and monitors.


ISOWATT218

## INTERNAL SCHEMATIC DIAGRAM



## ABSOLUTE MAXIMUM RATINGS

| Symbol | Parameter | Value | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\mathrm{CBO}}$ | Collector-Base Voltage $\left(\mathrm{I}_{\mathrm{E}}=0\right)$ | 1500 | V |
| $\mathrm{~V}_{\mathrm{CEO}}$ | Collector-Emitter Voltage $\left(\mathrm{I}_{\mathrm{B}}=0\right)$ | 700 | V |
| $\mathrm{~V}_{\text {EBO }}$ | Emitter-Base Voltage $\left(\mathrm{I}_{\mathrm{C}}=0\right)$ | 10 | V |
| $\mathrm{I}_{\mathrm{C}}$ | Collector Current | 10 | A |
| $\mathrm{I}_{\mathrm{CM}}$ | Collector Peak Current $\left(\mathrm{t}_{\mathrm{p}}<5 \mathrm{~ms}\right)$ | 20 | A |
| $\mathrm{I}_{\mathrm{B}}$ | Base Current | 5 | A |
| $\mathrm{I}_{\mathrm{BM}}$ | Base Peak Current $\left(\mathrm{t}_{\mathrm{p}}<5 \mathrm{~ms}\right)$ | 10 | A |
| $\mathrm{P}_{\text {tot }}$ | Total Dissipation at $\mathrm{T}_{\mathrm{C}}=25^{\circ} \mathrm{C}$ | 57 | W |
| $\mathrm{~T}_{\mathrm{stg}}$ | Storage Temperature | -65 to 150 | 150 |
| $\mathrm{~T}_{\mathrm{j}}$ | Max. Operating Junction Temperature | ${ }^{\circ} \mathrm{C}$ |  |

## THERMAL DATA

| $\mathrm{R}_{\mathrm{th} \text {-case }}$ | Thermal Resistance Junction-case | Max | 2.2 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| :--- | :--- | :--- | :--- | :--- |

ELECTRICAL CHARACTERISTICS ( $\mathrm{T}_{\text {case }}=25^{\circ} \mathrm{C}$ unless otherwise specified)

| Symbol | Parameter | Test Conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ices | Collector Cut-off Current ( $\mathrm{V}_{\mathrm{BE}}=0$ ) | $\begin{aligned} & \mathrm{V}_{\mathrm{CE}}=1500 \mathrm{~V} \\ & \mathrm{~V}_{\mathrm{CE}}=1500 \mathrm{~V} \quad \mathrm{~T}_{\mathrm{j}}=125^{\circ} \mathrm{C} \end{aligned}$ |  |  | $\begin{gathered} 0.2 \\ 2 \end{gathered}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| $I_{\text {ebo }}$ | Emitter Cut-off Current $\left(I_{C}=0\right)$ | $\mathrm{V}_{\mathrm{EB}}=5 \mathrm{~V}$ |  |  | 100 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {ceo(sus)* }}$ | Collector-Emitter Sustaining Voltage ( I c $=0$ ) | $\mathrm{Ic}=100 \mathrm{~mA}$ | 700 |  |  | V |
| Vebo | Emitter-Base Voltage $\left(I_{B}=0\right)$ | $\mathrm{I}_{\mathrm{E}}=10 \mathrm{~mA}$ | 10 |  |  | V |
| $\mathrm{V}_{\text {CE(sat) }}{ }^{*}$ | Collector-Emitter Saturation Voltage | $\mathrm{IC}_{\mathrm{C}}=7 \mathrm{~A} \quad \mathrm{I}_{\mathrm{B}}=1.5 \mathrm{~A}$ |  |  | 1.5 | V |
| $\mathrm{V}_{\mathrm{BE} \text { (sat) }}{ }^{*}$ | Base-Emitter Saturation Voltage | $\mathrm{I}_{\mathrm{C}}=7 \mathrm{~A} \quad \mathrm{I}_{\mathrm{B}}=1.5 \mathrm{~A}$ |  |  | 1.3 | V |
| $\mathrm{hfE}^{*}$ | DC Current Gain | $\begin{array}{lll} \hline \mathrm{I}_{\mathrm{C}}=7 \mathrm{~A} & \mathrm{~V}_{\mathrm{CE}}=5 \mathrm{~V} & \\ \mathrm{IC}=7 \mathrm{~A} & \mathrm{~V}_{\mathrm{CE}}=5 \mathrm{~V} & \mathrm{~T}_{\mathrm{j}}=10{ }^{\circ} \mathrm{C} \end{array}$ | $\begin{gathered} 6.5 \\ 4 \end{gathered}$ |  | 13 |  |
| $\begin{aligned} & \mathrm{t}_{\mathrm{s}} \\ & \mathrm{t}_{\mathrm{f}} \end{aligned}$ | RESISTIVE LOAD <br> Storage Time <br> Fall Time | $\begin{array}{ll} \hline \mathrm{V}_{\mathrm{CC}}=400 \mathrm{~V} & \mathrm{I}_{\mathrm{C}}=7 \mathrm{~A} \\ \mathrm{I}_{\mathrm{B} 1}=1.5 \mathrm{~A} & \mathrm{I}_{\mathrm{B} 2}=3.5 \mathrm{~A} \end{array}$ |  | $\begin{aligned} & 2.1 \\ & 140 \end{aligned}$ | $\begin{aligned} & 3.1 \\ & 210 \end{aligned}$ | $\begin{aligned} & \mu \mathrm{s} \\ & \mathrm{~ns} \end{aligned}$ |
| $\begin{aligned} & \mathrm{t}_{\mathrm{s}} \\ & \mathrm{t}_{\mathrm{f}} \end{aligned}$ | INDUCTIVE LOAD <br> Storage Time <br> Fall Time | $\begin{array}{ll} I_{\mathrm{C}}=7 \mathrm{~A} & \mathrm{f}=31250 \mathrm{~Hz} \\ \mathrm{I}_{\mathrm{B} 1}=1.5 \mathrm{~A} & \mathrm{I}_{\mathrm{B} 2}=-3.5 \mathrm{~A} \\ \mathrm{~V}_{\text {ceflyback }}=1200 \sin \left(\frac{\pi}{5} 10^{6}\right) \mathrm{t} \end{array}$ |  | $\begin{aligned} & 3.5 \\ & 320 \end{aligned}$ |  | $\begin{aligned} & \mu \mathrm{s} \\ & \mathrm{~ns} \end{aligned}$ |
| $\begin{aligned} & \mathrm{t}_{\mathrm{s}} \\ & \mathrm{t}_{\mathrm{f}} \end{aligned}$ | INDUCTIVE LOAD <br> Storage Time <br> Fall Time | $\begin{aligned} & \begin{array}{l} I_{\mathrm{C}}=7 \mathrm{~A} \\ \mathrm{I}_{\mathrm{B} 1}=1.5 \mathrm{~A} \\ \mathrm{~V}_{\text {ceflyback }}=1200 \sin \left(\frac{\pi}{5} 10^{6}\right) \mathrm{I} 2=-3.5 \mathrm{KHz} \\ \mathrm{I} \end{array} \quad \mathrm{~V} \end{aligned}$ |  | $\begin{aligned} & 1.7 \\ & 215 \end{aligned}$ |  | $\begin{aligned} & \mu \mathrm{s} \\ & \mathrm{~ns} \end{aligned}$ |

[^0]Safe Operating Area


Derating Curve


Collector Emitter Saturation Voltage


Thermal Impedance


DC Current Gain


Base Emitter Saturation Voltage


5

Power Losses at 32 KHz


Power Losses at 64 KHz


Switching Time Inductive Load at 32 KHz (see figure 2)


Switching Time Inductive Load at 64 KHz (see figure 2)


Reverse Biased SOA


## BASE DRIVE INFORMATION

In order to saturate the power switch and reduce conduction losses, adequate direct base current $\mathrm{I}_{\mathrm{B} 1}$ has to be provided for the lowest gain $h_{F E}$ at $T_{j}$ $=100^{\circ} \mathrm{C}$ (line scan phase). On the other hand, negative base current $\mathrm{I}_{\mathrm{B} 2}$ must be provided turn off the power transistor (retrace phase). Most of the dissipation, especially in the deflection application, occurs at switch-off so it is essential to determine the value of IB2 which minimizes power losses, fall time $\mathrm{tf}_{\mathrm{f}}$ and, consequently, $\mathrm{T}_{\mathrm{j}}$. A new set of curves have been defined to give total power losses, $t_{s}$ and $t_{f}$ as a function of $l_{B 2}$ at both 32 KHz and 64 KHz scanning frequencies in order to choice the optimum negative drive. The test circuit is illustrated in fig. 1.

Inductance $L_{1}$ serves to control the slope of the negative base current $\mathrm{I}_{\mathrm{B} 2}$ in order to recombine the excess carriers in the collector when base current is still present, thus avoiding any tailing phenomenon in the collector current.
The values of $L$ and $C$ are calculated from the following equations:
$\frac{1}{2} L\left(I_{C}\right)^{2}=\frac{1}{2} C\left(V_{C E f l y}\right)^{2}$
$\omega=2 \pi f=\frac{1}{\sqrt{L C}}$
Where $\mathrm{I}_{\mathrm{c}}=$ operating collector current, VCEfly= flyback voltage, $f=$ frequency of oscillation during retrace.

Figure 1: Inductive Load Switching Test Circuit.


Figure 2: Switching Waveforms in a Deflection Circuit.


| DIM. | mm |  |  | inch |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN. | TYP. | MAX. | MIN. | TYP. | MAX. |
| A | 5.35 |  | 5.65 | 0.211 |  | 0.222 |
| C | 3.30 |  | 3.80 | 0.130 |  | 0.150 |
| D | 2.90 |  | 3.10 | 0.114 |  | 0.122 |
| D1 | 1.88 |  | 2.08 | 0.074 |  | 0.082 |
| E | 0.75 |  | 0.95 | 0.030 |  | 0.037 |
| F | 1.05 |  | 1.25 | 0.041 |  | 0.049 |
| F2 | 1.50 |  | 1.70 | 0.059 |  | 0.067 |
| F3 | 1.90 |  | 2.10 | 0.075 |  | 0.083 |
| G | 10.80 |  | 11.20 | 0.425 |  | 0.441 |
| H | 15.80 |  | 16.20 | 0.622 |  | 0.638 |
| L |  |  |  |  | 0.354 |  |
| L1 | 20.80 |  | 21.20 | 0.819 |  | 0.835 |
| L2 | 19.10 |  | 19.90 | 0.752 |  | 0.783 |
| L3 | 22.80 |  | 23.60 | 0.898 |  | 0.929 |
| L4 | 40.50 |  | 42.50 | 1.594 |  | 1.673 |
| L5 | 4.85 |  | 5.25 | 0.191 |  | 0.207 |
| L6 | 20.25 |  | 20.75 | 0.797 |  | 0.817 |
| N | 2.1 |  | 2.3 | 0.083 |  | 0.091 |
| R |  |  |  |  | 0.181 |  |
| DIA | 3.5 |  | 3.7 | 0.138 |  | 0.146 |



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[^0]:    * Pulsed: Pulse duration = 300 ss, duty cycle 1.5 \%

